

# Trouble Shooting during Heavy Leakage from Urea Plant HP Loop

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**Abstract** - In high Pressure Urea reactor, sudden pressure drop by any reason can cause bulging of liner. In any reason (heavy leakage in HP section of urea plant, PSV popped etc.) the HP loop pressure goes to zero, then how to drain out urea /carbamate solution from HP loop without pressure to take shut down. At gravity, it is very difficult to drain out urea solution from 1½" line and also huge amount of effluent generation. The urea reactor is a typical gas liquid urea and ammonium carbamate reactor involving not only back mixing phenomenon but also significant aspect of heat and mass transfer between high corrosive vapors and liquid phase. Urea Reactor containing about 34-35 % Urea, 33-34 % ammonia, 14% CO<sub>2</sub> and rest is water. In M/S. Saipem process all the safety has been taken in account e.g. to protect the reactor in case a sudden pressure increases an automatic system has been provided with interlocks to stop the fluid inlet feed. The temperature profile is progressively rising inside the reactor due to density variation. In this article, all procedure described at zero kg/cm<sup>2</sup> pressure Feed in in Urea reactor as well as draining of urea solution to take shut down and how to manage effluent generation at draining of HP loop. The experience gained when our 31 stream HP loop PSV-2 (HP loop Carbamate separator PSV) suddenly popped with heavy leakage from upstream flange of PSV-2 on dated 11/10/2018 at 11.50 hrs. and pressure of HP loop went to zero kg/cm<sup>2</sup>. At that time the plant was running on full and constant load.

**Keywords** - Reactor Feed in, Reactor Draining, effluent generation, Safety hazards, trouble shooting, Pressure safety valve, corrosion.

## INTRODUCTION

National Fertilizers Ltd, (NFL) operates a fertilizer complex at Vijaipur, Distt. Guna (Madhya Pradesh), India consisting of two units Vijaipur-I and Vijaipur-II, plants were commissioned in December 1987 and March 1997 respectively. Ammonia Plants are based on M/s. HTAS's Steam Reforming of Natural Gas and Urea plants are based on M/S. Saipem's Ammonia Stripping technology. NFL, a

Schedule 'A' & a Mini Ratna (Category-I) Company. The Vijaipur unit, which is an ISO 9001:2000 & 14001 certified, comprises of two streams. The Vijaipur have two ammonia plant M/S. Haldor Topsoe Technology, Denmark capacity 1750 & 1864 TPD for Line-I & line-II respectively and four urea plant of M/S. Saipem ammonia stripping process, Italy. The capacity of Urea-I urea -II is 3030 & 3231 TPD respectively. The raw material used includes natural gas, water and power. Three Numbers Captive power plant of capacity 17 X 3 MW are used in this complex. The Complex manufactured about 2100000 MT urea per annum. The emergency situations which are likely to arise are several and extremely variable as to duration and seriousness. Considerable pressure and /or temperature increases Pipe line clogging because of crystallization. Sudden failure of services like PSV, flanges leakage failure of equipment's Fires, and / or ruptures with uncontrollable losses of toxic gasses. The evaluation of the seriousness of an emergency situation and therefore the decision of how to shut the plant down is a matter of the operators' experience. He should take prompt and corrective action. However, the inter lock system is designed to minimize the number of manual operations.

## Description of incident

On dated 11/10/2018 at 11.50 hrs the 31 stream was running on full load sudden loud sound heard and ammonia cloud observed near HP carbamate vessel. The PSV -2 (mounted on HP carbamate separator vessel) was popped and during popping upstream flange got heavy leakage of ammonia/carbamate as shown in the fig-2, 3 & 4 as trends of pressure drop. Immediately shut down of 31 stream was taken and control the situation. Now problem arise how to drain out the HP loop solution to arrest the leakage from the PSV? However, no casualty was there.

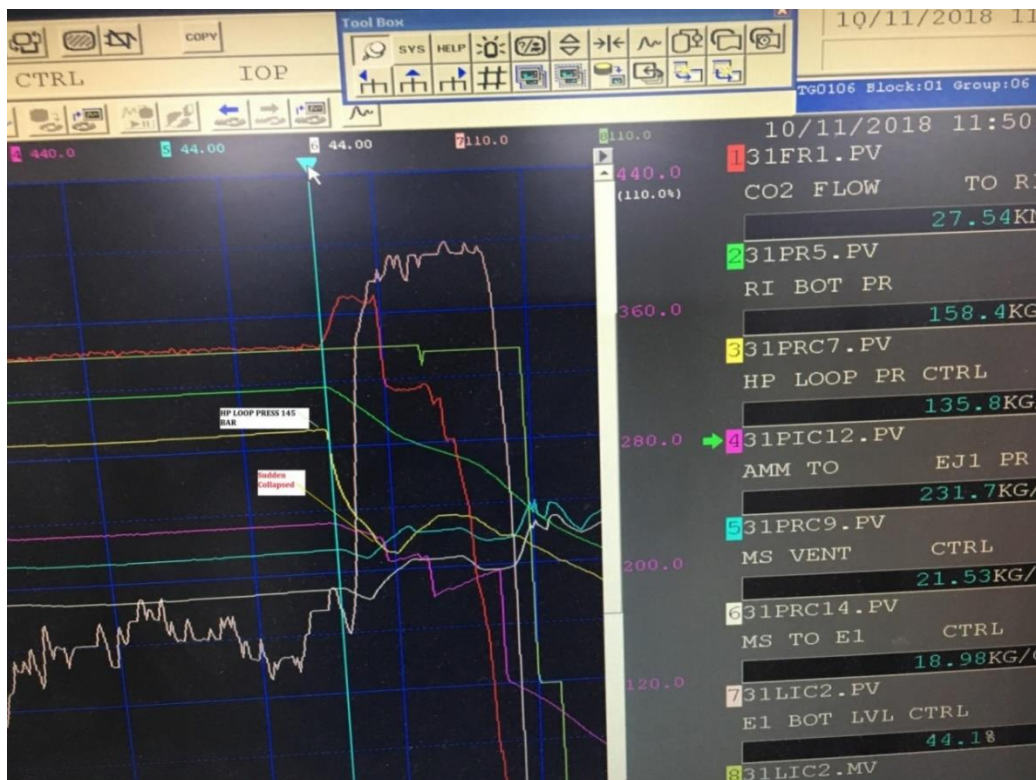


Fig-1(trends of Pressure when safety popped)



Fig-2(Trends of parameters when safety popped)

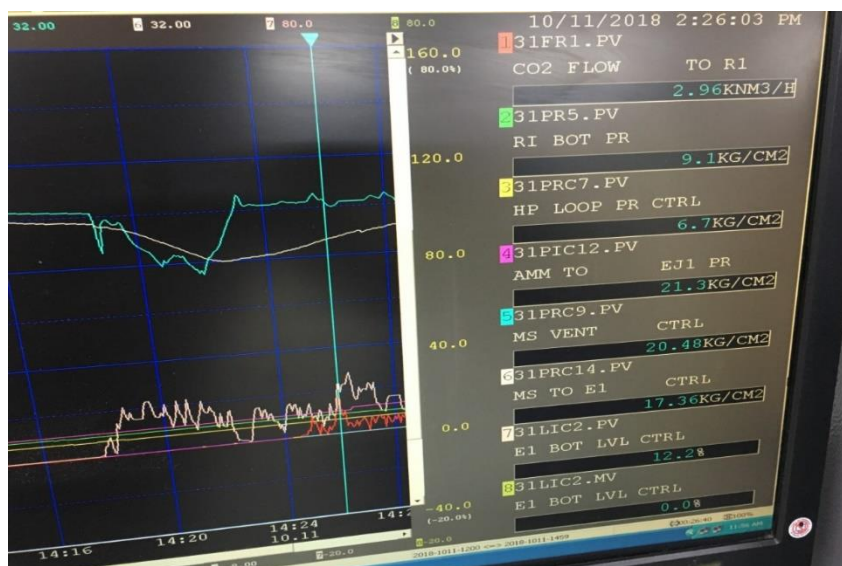


Fig-3(Trends of Parameters when safety popped)

HP loop form the centre of any urea plant. High pressures and temperatures, the corrosiveCircumstances and the health risks of ammonia in case of a leak put high demands to the integrity of such a vessel. At that condition anything could have happened, e.g. bulging of liner, leakage from weep holes, damage of liner, chances of casualty if the people were working there.

Sr. No.	Parameters	11.50 hrs	12.00 hrs	12.10 hrs	12.20 hrs	12.30 hrs
1	HP Loop Pressure (PIC 07)(kg/cm <sup>2</sup> )	135	110	66	25	4
2	Reactor bottom Temperature ° C	166	144	124	121	110
3	Reactor Top Temperature ° C	184	157	133	129	116

Table-1(Pressure & Temp profile at the time of PSV Popped)



Fig-4(Vapour & liquid, carbamate leakage from PSV-2)



As it is well knowing the modern urea processes are recycle type of process, therefore a temporary or sudden inefficiency of the synthesis loop, or more in detail of the urea reactor, would have a significant impact on the overall urea plant performances and under certain conditions may even lead to a plant shutdown. One of the challenges in operating a urea plant is to combat the corrosive process

environment in the High-pressure vessel in synthesis section.

After long discussion the decision was taken the upstream flange got tightened and PSV to be

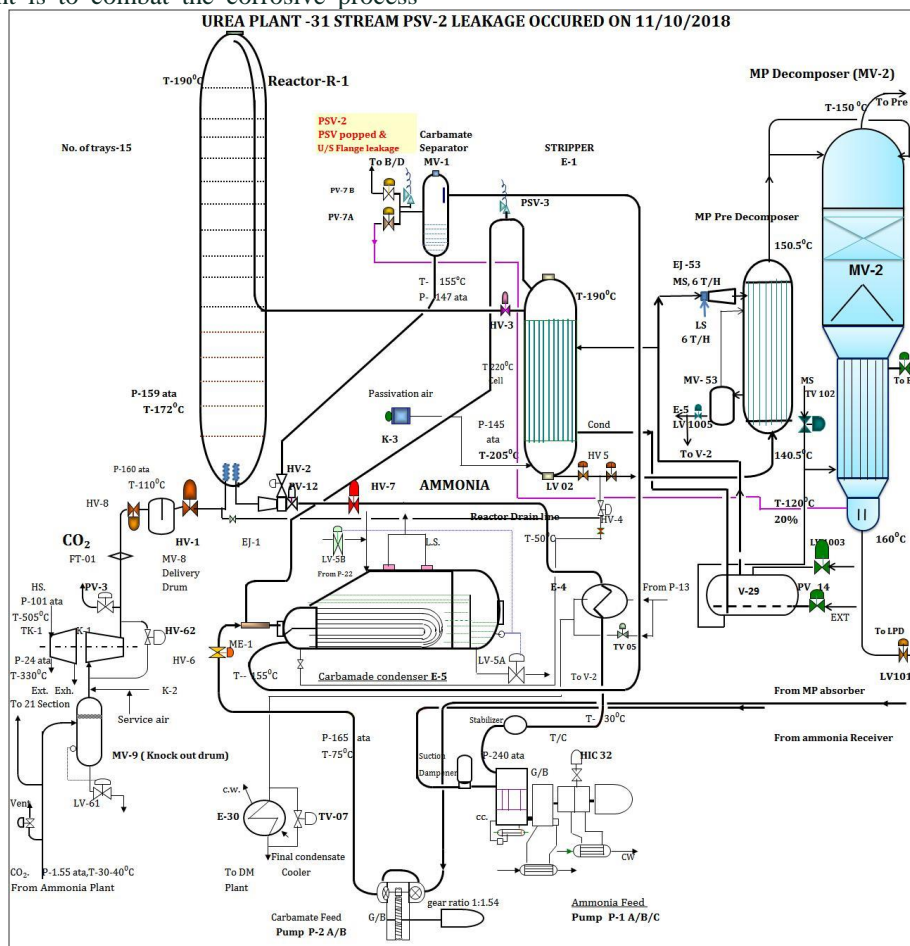


Fig-5 (HP loop, location of PSV-2 & 3)

Gaged. By using all safety equipment's (on line air mask, face shield etc.) the upstream flange of PSV -2 got tightened and PSV-2 gaged. Now for safety point of view this PSV was useless and fully depended on PSV-3(mounted on stripper vapors line).As the HP loop having two PSV one mounted on carbamate separator and other on stripper vapor line. Now problem of how to feed at zero kg/cm<sup>2</sup> pressure?

Now there are two option of filled reactor feed in at zero kg/cm<sup>2</sup> pressure.

1. The HP loop pressurized by ammonia start up line using jacketing steam.
2. First feed ammonia to reactor and after getting about 50 kg/cm<sup>2</sup> pressure CO<sub>2</sub> to be feed.

Sr. No.	15.00 hrs	15.30 hrs	16.00 hrs	16.30 hrs	17.00 hrs	17.30 hrs
Ammonia Feed in, m <sup>3</sup> /hr.	20	25	25	37	45	58
CO <sub>2</sub> Feed in, NM <sup>3</sup> /hr.	0	0	6800	9950	12000	15000
Reactor pressure kg/cm <sup>2</sup>	0	20	38	57	92	142
Reactor Top Temperature °C	116	129	155	178	183	190
Reactor Bottom Temperature °C	110	122	144	166	169	173

Table-2(Pressure & temp profile when reactor Feed at zero kg/cm<sup>2</sup> pressure)

In normal start up or feed in to the empty reactor is simple. The HP loop pressure increases by ammoniation at the rate of 30 kg/cm<sup>2</sup>/hr. The dedicated system is installed with pipe heat exchangers the ammonia pipe heated with 24 bar steam outside jacketed provision. The pipe is sufficient long so that the ammonia heated by this line about 150°C. when the pressure achieved about 90-100 kg/cm<sup>2</sup> and temperature 150°C, The Feed in of CO<sub>2</sub> and Ammonia through inlet main line to be fed.

But in present case the reactor is filled of liquid fluid with zero kg/cm<sup>2</sup> pressure and temperature about 120°C. Whenever start up to be performed with the filled reactor at zero kg/cm<sup>2</sup> plant and about 120° temperature equipment

shall be started to avoid liner damaged so the rate must be maintained at about 30kg/cm<sup>2</sup>/hr. Open steam to E-1 by PV-14 valve and rise temperature very slowly.

This is the challenging task to feed in the reactor. We have two ammonia High pressures feed pump M/S. Uraca made variable (with torque convertor) capacity 90 m<sup>3</sup>/hr. and one small pump M/S. Peroni made having capacity 25 m<sup>3</sup>/hr. fixed capacity with recycle valve. In this typical case, we were used small capacity pump for initial and after one hour high capacity pump was taken in line.

Plant Load %	MTPD	CO <sub>2</sub> TO R-1 (NM <sup>3</sup> /HR)	NH <sub>3</sub> TO R-1 (M <sup>3</sup> /HR)	P-1 (RPM)	NH <sub>3</sub> FROM BL (M <sup>3</sup> /HR)	Plant Load %	MTPD	CO <sub>2</sub> TO R-1 (NM <sup>3</sup> /HR)	NH <sub>3</sub> TO R-1 (M <sup>3</sup> /HR)	P-1 (RPM)	NH <sub>3</sub> FROM BL (M <sup>3</sup> /HR)
27.2	440	6860	25.9	30.9	17.0	85.8	1386	21610	81.6	95.8	53.4
28.6	462	7200	27.2	32.0	17.8	87.2	1408	21950	82.8	97.3	54.2
30.0	484	7550	28.5	33.5	18.6	88.5	1430	22300	84.1	98.8	55.1
31.3	506	7890	29.8	35.0	19.5	89.9	1452	22640	85.4	100.3	55.9
32.7	528	8230	31.1	36.5	20.3	91.2	1474	22980	86.7	101.8	56.8
34.0	550	8580	32.4	38.0	21.2	92.6	1496	23320	88.0	103.4	57.6
35.4	572	8920	33.7	39.5	22.0	94.0	1518	23670	89.3	104.9	58.5
36.8	594	9260	35.0	41.0	22.9	95.3	1540	24010	90.6	106.4	59.3
38.1	616	9600	36.2	42.6	23.7	95.6	1545	24118	91.0	107.0	59.6
39.5	638	9950	37.5	44.1	24.6	96.5	1560	24343	91.8	108.0	60.2
40.9	660	10290	38.8	45.6	25.4	97.4	1574	24569	92.7	109.0	60.7
42.2	682	10630	40.1	47.1	26.3	98.3	1588	24794	93.5	110.0	61.3
43.6	704	10980	41.4	48.6	27.1	99.2	1603	25019	94.4	111.0	61.8
44.9	726	11320	42.7	50.2	28.0	100.1	1617	25245	95.2	112.0	62.4
46.3	748	11660	44.0	51.7	28.8	101.0	1632	25470	96.1	113.0	62.9
47.7	770	12010	45.3	53.2	29.7	101.9	1646	25696	96.9	114.0	63.5
49.0	792	12350	46.6	54.7	30.5	102.8	1661	25921	97.8	115.0	64.1
50.4	814	12690	47.9	56.2	31.4	103.7	1675	26146	98.6	116.0	64.6
51.7	836	13030	49.2	57.8	32.2	104.6	1689	26372	99.5	117.0	65.2
53.1	858	13380	50.5	59.3	33.1	105.5	1704	26597	100.3	118.0	65.7
54.5	880	13720	51.8	60.8	33.9	106.4	1718	26823	101.2	119.0	66.3
55.8	902	14060	53.1	62.3	34.7	107.3	1733	27048	102.0	120.0	66.8
57.2	924	14410	54.4	63.8	35.6	108.2	1747	27273	102.9	121.0	67.4
58.6	946	14750	55.7	65.4	36.4	109.0	1762	27499	103.7	122.0	68.0
59.9	968	15090	57.0	66.9	37.3	109.9	1776	27724	104.6	123.0	68.5
61.3	990	15433	58.2	68.4	38.1	110.8	1791	27950	105.4	124.0	69.1
62.6	1012	15780	59.5	69.9	39.0	111.7	1805	28175	106.3	125.0	69.6
64.0	1034	16120	60.8	71.4	39.8	112.6	1819	28400	107.1	126.0	70.2
65.4	1056	16460	62.1	73.0	40.7	113.5	1834	28626	108.0	127.0	70.7
66.7	1078	16810	63.4	74.5	41.5	114.4	1848	28851	108.8	128.0	71.3
68.1	1100	17150	64.7	76.0	42.4	115.3	1863	29077	109.7	129.0	71.9
69.5	1122	17490	66.0	77.5	43.2	116.2	1877	29302	110.5	130.0	72.4
70.8	1144	17840	67.3	79.0	44.1	117.1	1892	29527	111.4	131.0	73.0
72.2	1166	18180	68.6	80.6	44.9	118.0	1906	29753	112.2	132.0	73.5
73.5	1188	18520	69.9	82.1	45.8	118.9	1921	29978	113.1	133.0	74.1
74.9	1210	18870	71.2	83.6	46.6	119.8	1935	30204	113.9	134.0	74.6
76.3	1232	19210	72.5	85.1	47.5	120.7	1949	30429	114.8	135.0	75.2
77.6	1254	19550	73.8	86.6	48.3	121.6	1964	30654	115.6	136.0	75.8
79.0	1276	19890	75.1	88.2	49.1	122.5	1978	30880	116.5	137.0	76.3
80.3	1298	20240	76.4	89.7	50.0	123.4	1993	31105	117.3	138.0	76.9
81.7	1320	20580	77.7	91.2	50.8	124.2	2007	31331	118.2	139.0	77.4
83.1	1342	20920	79.0	92.7	51.7	125.1	2022	31556	119.0	140.0	78.0
84.4	1364	21270	80.3	94.2	52.5						

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Table No.-3(Ratio of Ammonia and CO<sub>2</sub> at the feed in time)

We were using 2<sup>nd</sup> option we feed first ammonia at slow rate so we used small capacity ammonia feed pump 31 P-1C (cap-25 m<sup>3</sup>/hr.) after one hr. we have got about 35 kg/cm<sup>2</sup> pressure and after one hr. CO<sub>2</sub> fed to reactor and now normal filled reactor feed in conditions achieved. Urea

conversion reaction is slow and takes 20 minutes to attain equilibrium. The sufficient pressure is required for urea reaction. Considering the slowness of the reaction, urea reactor is so designed that residence time should be more than 20 minutes. Higher residence time favours equilibrium

conversion and normally reactors are designed for residence time of 30 minutes to one hour, depending upon other operating parameters. This exothermic reaction is slow at atmospheric pressure and room temperature, but almost instantaneous at a pressure of about 100 kg/cm<sup>2</sup>a and temperature of 150° C. Rate of formation of carbamate depends on the temperature and pressure. The rate increases with both temperature and pressure. At constant pressure, the rate increases with temperature, reaches the maximum and then rapidly decreasing up to zero value at the temperature corresponding to which the dissociation

pressure equals the working pressure. The heat of formation must be dissipated in order to avoid the increase of temperature which corresponds to a dissociation pressure equal to the working pressure. This is an equilibrium reaction and proceeds only in the liquid or solid phase. Rate of transformation of ammonium carbamate to urea without excess water or ammonia and NH<sub>3</sub>:CO<sub>2</sub> ratio of 3.5:1 indicates that for carbamate conversion to urea increases with temperature. At a temperature of approximately 170° C, equilibrium is reached within 20 minutes.

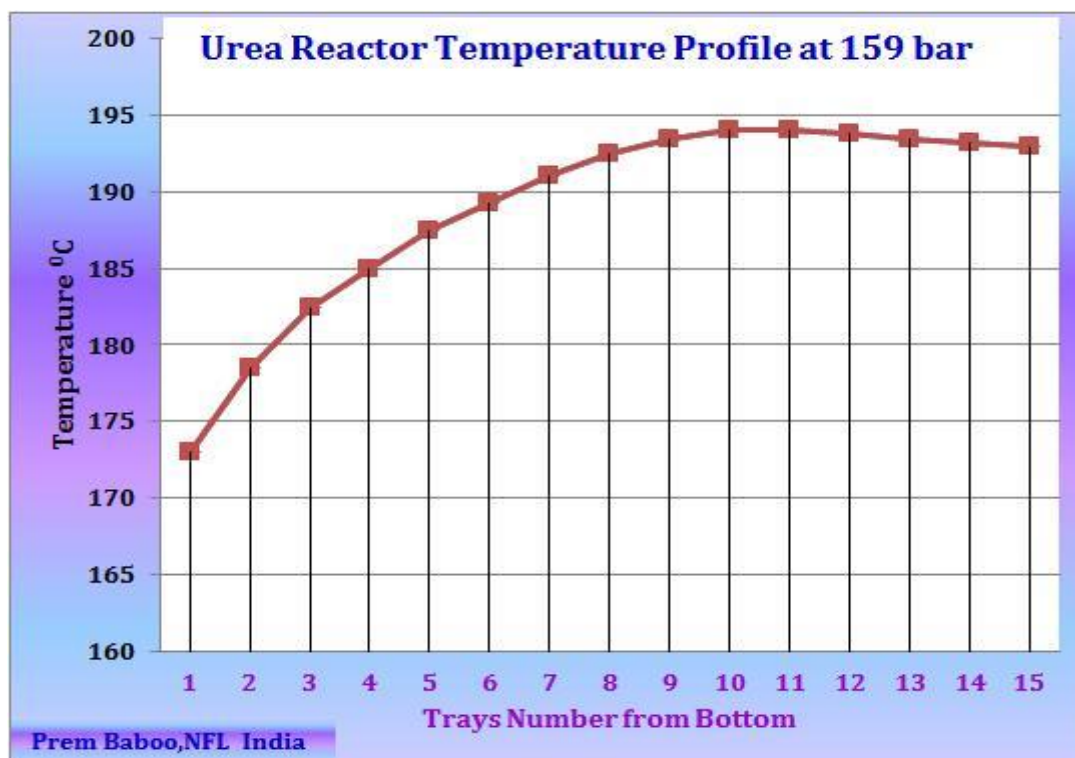


Fig-6(Temperature profile inside the reactors)

Slowly overflow of reactor appeared in stripper bottom and adopted normal rout of plant startup.  
How to drain out Urea/Carbamate solution from Urea Reactor at Zero Kg/cm<sup>2</sup> Pressure

In our case the leakage from PSV upstream flange had been arrested successfully but in case if leakage cannot be arrested then how to drain out HP loop solution at zero kg/cm<sup>2</sup> pressure. It is very typical task to handle the effluent generation as well as draining from 1½" drain line. From this line there are chances of choking the line frequently. In that case following procedure to be followed as per figure No. 7.

#### Procedure

First of all, start up jacketing line which is connected to Stripper vapour line with Isolation and NRV takes in line and medium pressure steam(MS) to be charged. Now HP

ammonia Feed pump starts and pressure to maintained at about 50 kg/cm<sup>2</sup> with the help of recycle line. Now ammonia feed to stripper vapour line and temperature of ammonia to be maintained at about 150°C. The pressure of HP loop gradually increases and when this reaches about 30-35 kg/cm<sup>2</sup> then draining of HP loop to be started from reactor bottom from CO<sub>2</sub> line as shown in the figure-7. total liquid must be drained through this line and pressure of HP loop to be maintained more than MP loop all urea solution collected Urea solution tank(V-5) and carbamate to be collected in carbonate solution tank(V-3). which should be reclaimed when plant normal running condition. As and when solution level becomes zero i.e. opening of LV-101(MP level controller) goes to zero then the system to be depressurized through PV-7 B. Now normal route LS purging and job hand over to mechanical maintenance for PSV replacement and leakage attending. There is no man entry so there is no need to filled water.



## DRAINING OF H.P.LOOP AT ZERO KG/CM<sup>2</sup> PRESSURE AND SOLUTION FILLED REACTOR

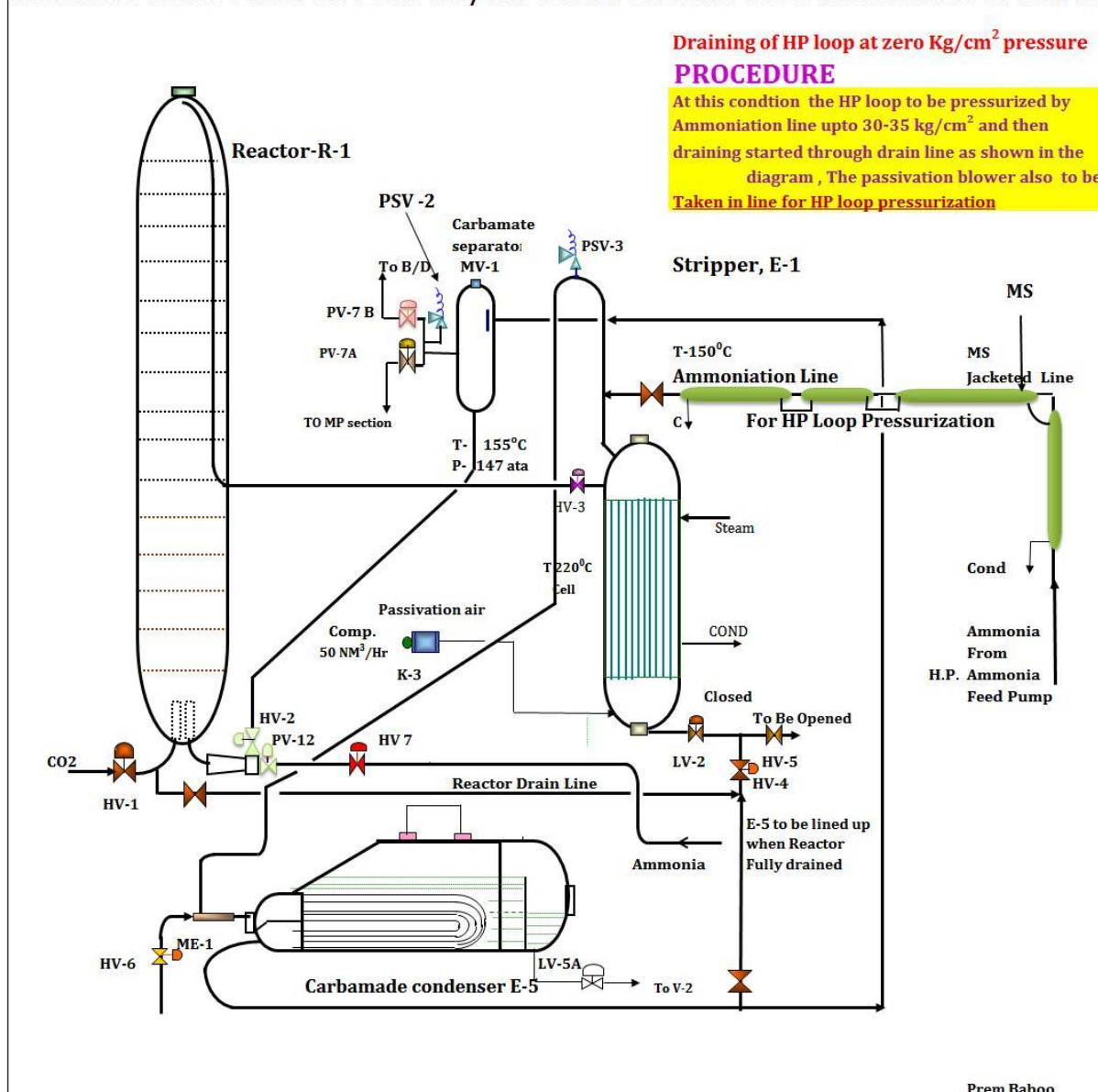


Fig-7(HP loop Draining as zero kg/cm<sup>2</sup> pressure)

Ammonia/carbamate vapour can easily remove with low pressure steam about 3-4 hrs. PPE can be used for this purpose. Ammonia should be checked by opening any vent/drain line, if ammonia smells coming then further LS purging for one hour to be done.

### Carbamate PSV monitoring

In practice, all the carbamate PSV d/s steam must be opened in blow down line because in case of PSV passing, carbamate vapour easily crystalized in solid form resulting the B/d header will have choked & lead to line blast. The B/D header is not designed for high pressure. So, the steam valve must be checked and opened and lines should be hot.

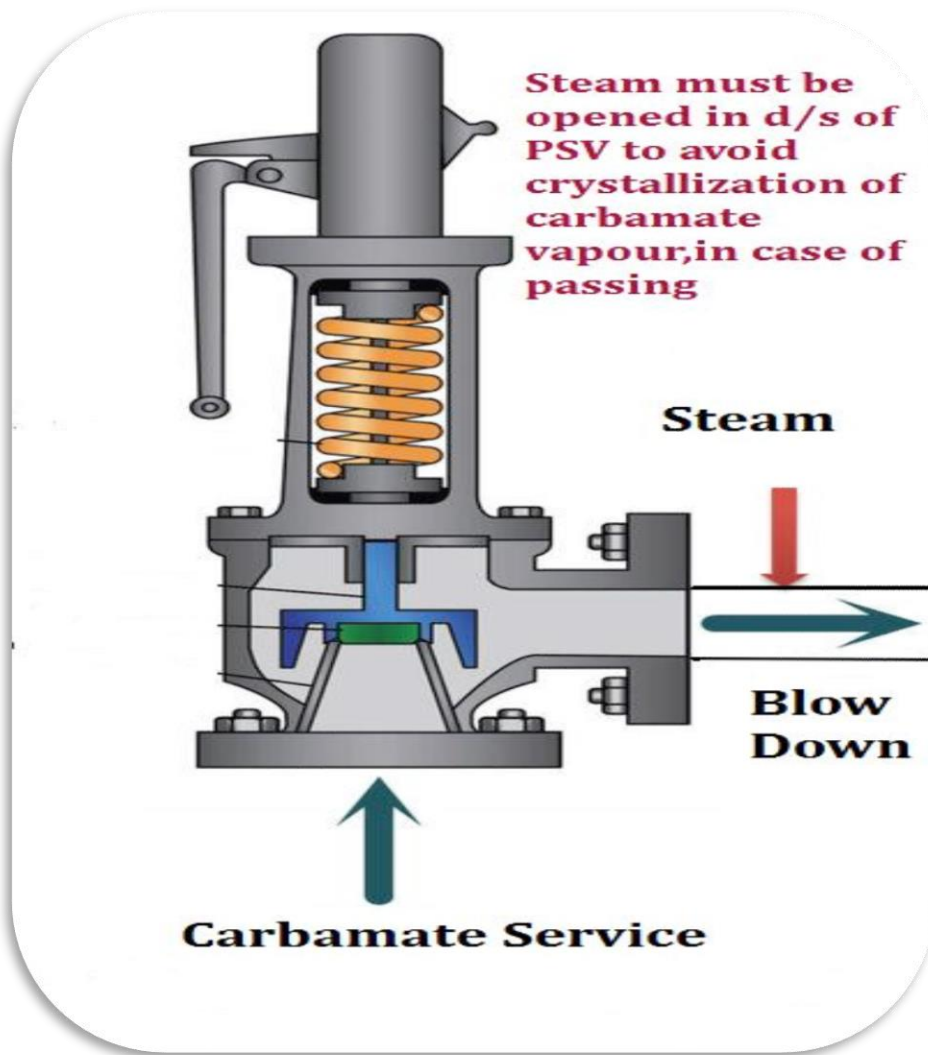


Fig-8 (PSV mounted in HP loop in carbamate vapour)

#### CONCLUSION

Safety rules should never be denied. Continuously confirm and share the consensus that “Safety takes precedence over all other Considerations,” and realize and maintain safe, sanitary conditions in all workplaces. Strive to complete all jobs with no accidents and no harm to people by enforcing preventive safety measures. Ammonia is one among the largest volume inorganic chemicals in the chemical process industries and used mainly for production of fertilizers using steam reforming of natural gas. But problems and failures do occur frequently in the ammonia plant even after following the inherently safer design philosophy and risk assessment. Major areas of concerns/ failures are reforming and urea synthesis loop causing fires/leakages and shutdowns. Ensure information security, and take appropriate safeguards against threats and risks to business assets. Minimize environmental burden by saving resources and energy, detoxifying, reducing and recycling waste, and by preventing pollution during the course of our work duties. Establish and continuously improve the effectiveness of management systems, including objective setting, hazard identification, risk evaluation, determination of countermeasures, execution control and review, and education and training, in

line with management system belief that the securement of HSSE and quality is a prerequisite for business continuity.

#### Legends-

HP high pressure, PPE-personal protective equipment's. MW-megawatt, HSSE-health Safety Security and environment. LS-low pressure steam, MS medium (24 bar) steam. B/D-Blow down.