Performance Characteristics of Magnetic Abrasive Finishing (MAF) of Al 4061

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Abstract—Magnetic abrasive finishing (MAF) is one of the most important final machining processes, and the performances of finishing media play an important role in the finishing effects and efficiency. In this paper, a new magnetic finishing media with semi-solid state was presented and prepared, and finishing setup for the outer rotary surface was developed. In order to determine the optimum angle between N pole and S pole, simulation was performed using ANSYS Maxwell 14.0. MRR as a function of magnetic flux density, mass ratio, rotational speed of magnetic poles and diameter of abrasive particles and ferromagnetic particles. Finishing experiments of main parameters on materials removal ratio MRR was examined. Experimental results indicated that the percentage change % in the material removal and surface roughness amount increased with the increase of the rotational speed, the mesh number of the abrasive particles, and the mass ratio of base polymer, ferromagnetic phase and abrasive phase.

Keywords—Magnetic Abrasive Finishing; Orthogonal Array

Introduction

Magnetic abrasive finishing (MAF) is one of the advanced finishing processes, which produces a high level of surface quality and is primarily controlled by a magnetic field. In MAF, the work piece is kept between the two poles of a magnet. The working gap between the work piece and the magnet is filled with magnetic abrasive particles. A magnetic abrasive flexible brush (MAFB) is formed, acting as a multipoint cutting tool, due to the effect of the magnetic field in the working gap. When inserting a cylindrical work piece in such a processing field giving revolution, feed and vibration in axial direction, surface and edge finishing are carried out by magnetic brush. In the application of ferromagnetic substance of work, for instance, work piece is also magnetized and the magnetic force acts on the top of the brush between the work piece and the abrasive grains resulting in pressing the abrasive grains to work surface. The MAF process removes a very small amount of material by indentation and rotation of magnetic abrasive particles in the circular tracks. High quality and limited dimensional tolerance parts used in the aircraft. automobile, and shipbuilding industries require excellent surface finish. Conventional methods such as filling, lapping, honing, super finishing, grinding, polishing and buffing are used to modify the surface texture produced by manufacturing process. To further optimize the finishing operation unconventional machining processes like MAM are gaining attention owing to their ability to provide better surface finish than the conventional processes. Magnetic abrasive machining (MAM) is a process in which a magnetic power is employed as a machining force. This force is directing the abrasive particles towards the target surface. The efficiency of the process is easily controllable by the electric current. To prevent the over-finishing of surface roughness, careful monitoring of the process automation is needed. Therefore, MAM has been used for accuracy of surface finishing because of many advantages such as self-adaptability, controllability and self-sharpening.

Various industrial applications require very high surface finish up to the range of nanometres or even above with the development of modern manufacturing trends. Presently, it is required that the parts, used in manufacturing semiconductors, atomic energy parts, medical instruments and aerospace applications, have a very fine surface roughness. Amongst them, vacuum tubes, wave-guides and sanitary tubes are difficult to be polished by conventional finishing methods such as lapping, because of their shapes. The technology for super finishing needs ultra clean machining of advanced engineering materials such as silicon nitride, silicon carbide, and aluminium oxide which are used in high-technology industries and are difficult to finish by conventional grinding and polishing techniques with high accuracy, and minimal surface defects, such as micro cracks. Therefore, magnetic abrasive finishing (MAF) process has been recently developed for efficient and precision finishing.

With the development of high-end equipment, there are a large number of components having high performance, which require good surface layer structure, high surface quality, mechanical and physical properties. Their surface quality directly affects the service performance and service life of the equipment. For example, the surface quality of the very low friction hydraulic valve spool and valve sleeve has a direct impact on assembly quality, sealing and service performance.

Magnetic abrasive finishing (MAF) is one of the nontraditional machining processes, which can realize the decrease of surface roughness value and improvement of wear resistance and mechanical properties by interaction and relative motion between the media and the work piece. MAF has been used to finish solid or hollow cylindrical parts and flat workpieces and it was investigated from finishing mechanism, process parameters, material removal and surface integrity by many researches and reported the internal finishing of stainless steel tubes and determined the finishing effects. Reported the development of a typical internal finishing process by applying magnetic abrasives using a pole rotation system and investigated the finishing process for alumina ceramic components and austenitic stainless steel capillary tubes investigated the ultra-precision finishing of the inner surface of ceramic tube using MAF. Explored the application of low frequency alternating magnetic field for imparting surface modification of brass tube. Developed a setup used for finishing Para/diamagnetic flat workpieces with different hardness values and compared the finishing characteristics of two paramagnetic materials.

Developed a mathematic model of surface roughness Ra as a function of work piece material properties and process factors. Proposed a new ultra-precision MAF process using low frequency alternating magnetic field and investigated the effects of alternating magnetic field on magnetic field distribution, finishing force and abrasive behavior. Explored a pulsating direct current to the electromagnet to create a stirring effect on the flexible magnetic abrasive brush, and reported an obvious improvement in surface roughness over the conventional processes in which a static direct current was applied to the electromagnet. Developed a novel tool based on MAF principle for finishing holes, blind holes, grooves and vertical surfaces, and evaluated the finishing performance by experimental study. Investigated the inter-relations of key finishing parameters by using a dual magnetic roller tool and a 6-axis robot arm the influence of three vibration modes on the polishing effectiveness and studied the effect of types and size of abrasive on surface finishing reported ultrasonic assisted magnetic abrasive finishing.

(U MAF) and measured the machining forces in case of MAF and UAMAF. Reported UAMAF and discussed material removal mechanism, then developing a mathematical model predicting the material removal ratio (MRR). Reported a new media based on viscoelastic carrier and investigated the improvement of surface roughness Ra for finishing aluminum workpieces. The maximum improvement in surface roughness Ra is 23 % investigated the effects of some parameters on surface roughness Ra for aluminum sheet with MAF, and the maximum decrease value Ra in surface roughness Ra is 0.267 reported the development of new vibration assisted cylindrical-magnetic abrasive finishing (VAC-MAF) setup. The material removal and the decrease of surface roughness Ra for improved approximately by 100 % and 150 %, respectively, as compared to MAF without vibration. A hybrid process combining electrochemical machining and MAF. which was used to process Al 6061. The surface roughness Ra decreased from 1.3 µm to 0.2 µm. Developed a new MAF setup for finishing internal spiral grooves of a cylindrical tube and analyzed the finishing mechanism. the effect of the process parameters on surface roughness Ra for aluminum specimen was investigated, and microscopic surface profiles demonstrate 70 % improvement in the surface roughness Ra. All the studies focus on finishing mechanism, process parameters, the magnetic field improvement, finishing effects and hybrid process. The literatures about the property improvement of the media were rarely reported.

In MAF, finishing media used at present are almost powder media. This kind of finishing media is easy to escape from the finishing zone, and its availability is extremely low.

In view of the above, in this study, we prepared a kind of which magnetic finishing media has viscoelastic characteristics, that is, the deformation properties of this media have the characteristics of both solid elasticity and liquid viscosity under the action of external force, and its mechanical properties change with time, called as the mechanical relaxation phenomenon. The new finishing media show semi-solid state, having good magnetic conductivity and fluidity, and this resilient multipoint cutting tool has the flexibility to deform itself in conformity to the shape of workpiece surface and can be used to remove materials from complicated geometries.

II. EXPERIMENTAL SET UP A. Design of NdFeb Magnetic Holding Fixture

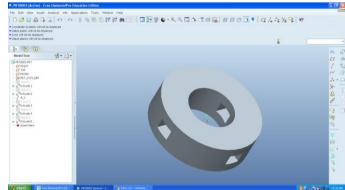


Fig 1 Creo-Magnet Holding Fixture



Fig.2. Fabricated Magnet Work Holding Device

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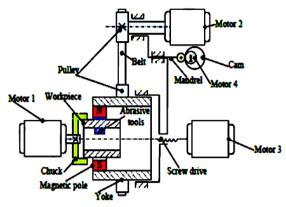


Fig.3 Experimental Setup

The setup includes four motors, belt drive, magnetic field generator, cam mechanism, screw mechanism and automatic control system. Motor 1 drives the workpiece rotating. The magnetic field generator is composed of NdFeB magnets (that is magnetic poles) and yoke, and NdFeB permanent magnets are mounted on the yoke. The number and the radial or circumferential position of magnets can be changed in order to alter magnetic flux density. Motor 2 drives the magnetic field generator rotating by the belt drive. Motor 3 drives the magnetic field generator moving along the axial direction of the workpiece by screw mechanism. Motor 4 drives the magnetic poles realizing vibrations along the axial direction of the workpiece by cam mechanism. When the media are placed in the inner surface of the workpiece or the gap between the workpiece and magnetic poles, they would attach to the workpiece surface due to the action of the strong magnetic force. When the magnets and/or the workpiece move, surface finishing of the workpiece would be achieved.

Table 1 Details of Simulation

Factors	Magnitude
Shape of magnetic poles	Rectangular Shaped
Inner diameter of magnetic poles	50 mm
Outer diameter of magnetic poles	150 mm
Thickness of magnetic poles	10 mm
Material of magnetic poles	N40 NdFeB
Angle θ between N pole and S pole	90°
Diameter of workpiece	25 mm
Length of workpiece	120 mm
Material of workpiece	4061 Aluminium alloy

Table 2 Properties of N40 NdFeB permanent magnetic poles

Remanence strength	Coercive force	Intrinsic coercivity	Maximum energy product	Maximum operating temperature
mT	kA/m	kA/m	kJ/m3	°C
1250-1280	≥ 923	≥ 955	≥ 318-342	80

Table 3 Details of experimental conditions

Factors	Magnitude
Workpiece hardness	80 HB
Density of workpiece	2.8 g/cm3
Diameter of abrasive particle	0.048 mm
Diameter of ferromagnetic particle	0.15 mm
Thickness of magnetic poles	10 mm
Relative permeability of abrasive particle	0.999996
Relative permeability of ferromagnetic	1350
particle	
Relative permeability μ0	4×10-7 H/m
Magnetic flux intensity B	0.45 T
Rotational speed of magnetic poles	346, 516, 792

Diameter of workpiece	25 mm
Mass ratio of base polymer, abrasive phase	2:1:1, 3:2:1, 4:3:1
and ferromagnetic phase	



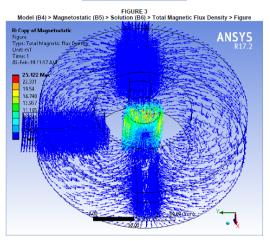


FIGURE 4
Model (B4) > Magnetostatic (B5) > Solution (B6) > Total Magnetic Flux Density > Figure 2

Fig.3. Ansys total magnetic flux density

III. EXPERIMENTAL RESULTS AND DISCUSSION The Table 4 shows the machining parameters such as

Rotation of Magnetic Poles, Mass Ratio, Abrasive mesh size and their levels for the machining Al 4061.

Table 4 Machining Parameters and their levels

S.No	Control Parameters	L1	L2	L3
1	Mass Ratio	2:1:1	3:2:1	4:3:1
2	Rotation of Magnetic	346	516	792
	Poles (rpm)			
3	Abrasive Mesh size	100	200	225
	(Sic, Grit)			

A. Degress of freedom

The number of comparisons that needs to be made to determine which level is better. For example, a four level parameter has three degree of freedom. The Orthogonal array is selected based on the degrees of freedom.

B. Selection of Orthogonal Array

Calculated degrees of freedom = 6 < 9 and which is closer to L₉.So, for the present analysis, an L9 orthogonal array with three columns and nine rows is used. Only nine experiments are required to study the entire machining parameters using the L₉ orthogonal array.

C. L₉ Orthogonal Array

Calculated degrees of freedom is 9 and which is closer to L_9 .So, for the present analysis, an L_9 orthogonal array with three columns and nine rows is used which is shown in Table 5.

Table 5 L₉ Orthogonal array

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S.No	Mass Ratio	Rotation of Magnetic Poles (rpm)	Abrasive Mesh Size
1	1	1	1
2	1	2	2
3	1	3	3
4	2	1	2

5	2	2	3
6	2	3	1
7	3	1	3
8	3	2	1
9	3	3	2

Table 6 shows the orthogonal array with values such as Rotation of Magnetic Poles, Mass Ratio, Abrasive mesh size for conducting the experiments on Magnetic Abrasive Machining.

Table 6 L₉ Orthogonal Array with Values

S.No	Mass Ratio	Rotation of	Abrasive Mesh
		Magnetic Poles	Size
		(rpm)	
1	2:1:1	346	100
2	2:1:1	516	200
3	2:1:1	792	225
4	3:2:1	346	200
5	3:2:1	516	225
6	3:2:1	792	100
7	4:3:1	346	225
8	4:3:1	516	100
9	4:3:1	792	200

The experimental observations are planned in such a way for conducting fruitful research analysis for deriving the effective research findings, which could be useful to the applied researchers and manufacturing industries in the area of micromachining achieved through MAF. To analyze the control of the desired performance characteristics of the process parameters of the Magnetic Abrasive Finishing system, a scheme was designed so as to properly utilize the developed MAF set-up.

All the experiments were carried out on 4061 aluminum alloy. The amount of the media is was 40 g. The diameter of all the workpiece was 25 mm so that the samples could keep suitable gap with the magnetic poles. For experimentation, the workpiece was held rigidly on the experimental setup with the help of three jaw chuck.

Initial and final weights of the jobs were taken by a precision electronic weighing machine. MRR was calculated as the material removed, i.e. the difference of initial and final weight per unit machining time. The standard machining time for each experiment is 30 min.

D. Experimental results for MRR and surface roughness

Table 6 Experimental Results of MRR

S.No	MRR (gm)		MRR	MRR
		(8)	(gm)	
	Before	After	Diff	mm ³ /min
	Machining	Machining		(10^{-6})
1	142.740	142.708	0.032	1.067
2	139.602	139.515	0.087	2.9
3	142.936	142.104	0.832	0.277
4	140.927	140.899	0.028	93.33
5	141.768	141.386	0.382	0.127
6	141.976	141.137	0.839	0.279
7	140.637	140.601	0.036	1.2
8	142.952	142.893	0.059	1.97
9	142.033	140.955	1.078	0.359

Table 7 Experimental Results of Surface Roughness

S.No	Surface Rougness (Ra, µm)
1	0.65
2	1.83
3	1.63
4	1.08
5	0.8
6	1.09
7	1.69
8	1.54
9	1.4

IV. OPTIMIZATION

In order to assess the effect of each machining parameters on the Process ,the Taguchi approach was used. This method is a type of Statistical technique called Design of Experiments (DOE) that makes it possible to analyze the effect of more than one factor at the same time while reducing the number of experiments. Thus using the Taguchi approach, the design of experiments and analysis of results can be done with less effort and expenses. However, since the method considerably reduces the number of experiments, quality loss of results could appear.

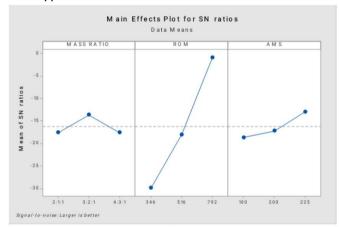


Fig.4. S/N ratio of MRR

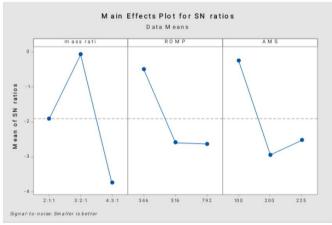


Fig.5. S/N ratio of Ra

The best machining condition to achieve better MRR & Lower Surface roughness is 3:2:1, 792 rpm, 225 μ m & 4:3:1, 792 rpm, 200 μ m.

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CONCLUSION

This paper presents a newly developed media and its material removal model. The main conclusions are deduced as follows:

The magnetic flux density increases first and then decreases with the increase of the angle between N pole and S pole. When the angle is 90°, the magnetic flux density is the maximum and finishing capacity of the media is high. Therefore, the optimum angle between N pole and S pole is 90°. It is established theoretically that the MRR is a function of the rotational speed, the mass ratio and the mesh number of abrasive particles. The MRR model is validated by the experiment. With the increase of the rotational speed and the mesh number of abrasive particles, the % Ra and the MRA increased. With the mass ratio of base polymer, ferromagnetic phase and abrasive phase is 4:3:1, the % Ra reaches the maximum of 94.85 %, and the MRR reaches the maximum of 1.85 mg/s. This finishing process could not only be used to finishing the outer surface or inner surface of small tube, but also be used to finishing large tube and special components such as deep groove and narrow slit by adjusting the size and position of the magnetic poles. However, this process has a certain limitation being used to finish blind hole due to small force. The roughness and tolerance band of component achieved using control parameter Magnetic Abrasive Machining (MAM) for polishing of cylinder work piece was developed using available abrasives.

The experimentation with these process parameters reduced the surface roughness value on a cylindrical component from an initial Ra value. These studies also indicated the need to consider the work piece initial roughness, apart from its hardnessfor achieving an improved finish on the work surface. Study shows that on various parameters improvement insurface finish is maximum in case of brass as compared to other materials.

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