# Load Flow Analysis of IEEE-3 bus system by using Mipower Software

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Abstract— The load flow study or power flow analysis is very important for planning, control and operations of existing systems as well as planning its future expansion. The satisfactory operation of the system depends upon knowing the effects of interconnections, new loads, new generating stations or new transmission lines etc., before they are installed. It also helps to determine the best size and favorable locations for the power capacitors both for the improvement of the power factor and also raising the bus voltage of the electrical network. They help us to determine the best locality as well as optimal capacity of the proposed generating stations, substations or new lines.

1) For this work the gauss-seidel method is used for numerical analysis. Nowadays Mipower software is used for load flow studies. This type of analysis is useful for solving the power flow problem in different power systems which will useful to calculate the unknown quantities.

Keywords-Power flow analysis, Power capacitors, Optimal capacity ,Guass-siedel method,Mipower software

## I. INTRODUCTION

The Load flow problem consists of calculation of voltage magnitude and its phase angle at the buses. And also the active and reactive lines flow for the specified terminal or bus conditions.

Load flow studies are used to ensure that electrical power transfer from generators to consumers through the grid system is stable, reliable and economic. Conventional techniques for solving the load flow problem are iterative, using the Newton-Raphson or the Gauss-Seidel methods. Depending upon the quantities specified for the buses, they are classified into three types namely load bus, generator bus or voltage controlled bus and slack bus or swing bus or reference bus.

## II. BUS CLASSIFICATION

Buses are classified according to which two out of the four variables are specified

•Load bus: No generator is connected to the bus. At this bus the real and reactive power are specified and it is desired to find out the volatage magnitude and phase angle through load flow solutions.It is required to specify only Pd and Qd at such bus as at a load bus voltage can be allowed to vary within the permissible values.

- •Generator bus or voltage controlled bus: Here the voltage magnitude corresponding to the generator voltage and real power Pg corresponds to its rating are specified. It is required to find out the reactive power generation Qg and phase angle of the bus voltage.
- ulletSlack (swing) bus: For the Slack Bus, it is assumed that the voltage magnitude |V| and voltage phase are known, whereas real and reactive powers Pg and Qg are obtained through the load flow solution

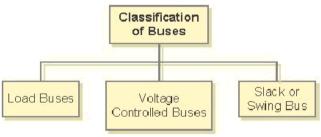
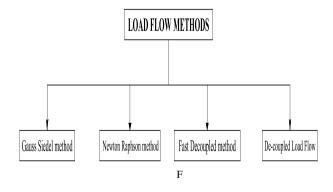


Fig.1 Bus classification

# III. SOLUTION METHODS

The solution of the simultaneous nonlinear power flow equations requires the use of iterative techniques for even the simplest power systems.

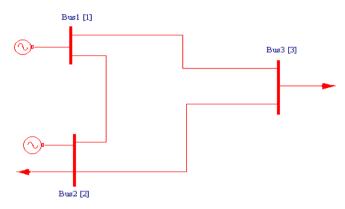
There are many methods for solving nonlinear equations, as shown in Fig.2



ig.2 Types of Load flow methods

## IV. IEEE 3 BUS SYSTEM STABILITY

Figure shows a single line diagram of a 3 bus system with two generating units, three lines. Perunit transmission line series impedances and shunt susceptances are given on 100 MVA base in Real power generation, real and reactive power loads in MW and MVAR are give. Conduct the load flow analysis...



Assume the base voltage for the bus as 11 kV and system frequency as 50 Hz.

Impedances and line charging for the system

Table: 1.1		
Bus code	Admittance	Line charging
From - To	Ypq	Y'pq/2
1-2	1.47+j5.88	J0.015
1-3	2.94-j11.77	j0.07
2-3	2.75-j9.17	j0.04

# Generation, loads and bus voltages for the system

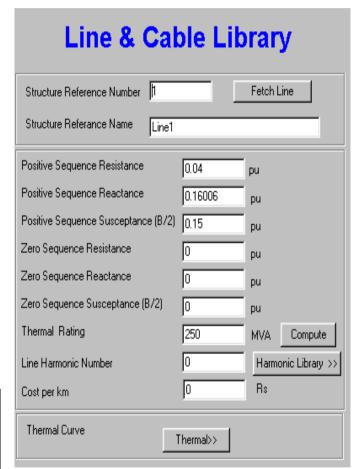
Τ	`able : 1.2				
В	Bus	Generat	Generation	Load	Load
us	Voltage	ion	MVAR	MW	MVA
N		MW			R
0					
1	1.04+j0.0	0	0	0	0
2	1.02+j0.0	100		50	20
3	1.00+j0.0	0	0	250	150
	-				

#### Transmission Line Element Data

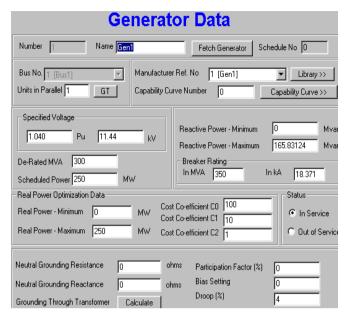
Line No	From Bus	To Bus	No. of circuits	Structure Ref. No.
2	1	3	1	2
3	2	3	1	3

Bus code No	Intertia(H)	Xd'
1	160	0.1
2	3	0.3

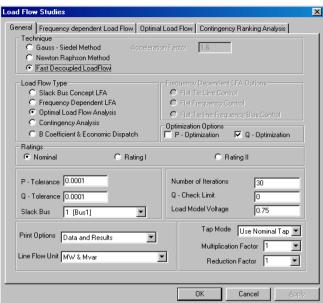
Line and cable Library



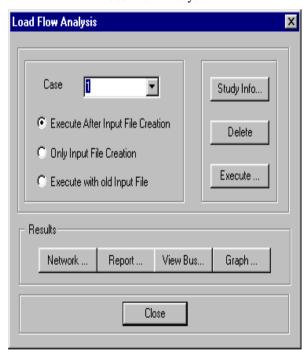
## Generator Data



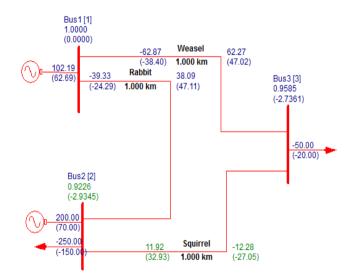
## Load flow studies



# Load Flow Analysis



Load flow analysis taken here for case study of IEEE-3 bus system. The network shown in Figure-3 a single line diagram is prepared using Mi-Power software. Execute load flow analysis and click on Report in load flow analysis dialog to view report.



V.	SUMMARY OF RESULTS:	NOMINAL SYSTEM FREQUENCY (Hzs): 50.000000		
	- Date and Time: Fri Oct 17 12:23:30 2014	FREQUENCY DEVIATION (Hzs): 0.000000		
		FLOWS IN MW AND MVAR, OPTION: 0		
	LOAD FLOW ANALYSIS	SLACK BUS : 0		
	CASE NO: 1 CONTINGENCY: 0 SCHEDULE NO: 0	(MAX GENERATION BUS) TRANSFORMER TAP CONTROL OPTION		
	CONTINGENCY NAME : Base Case	: 0		
	RATING CONSIDERED : NOMINAL	Q CHECKING LIMIT (ENABLED) : 4		
		REAL POWER TOLERANCE (PU)		
	VERSION NUMBER: 7.3 %% First Power System Network	: 0.00100 REACTIVE POWER TOLERANCE (PU) : 0.00100		
	LARGEST BUS NUMBER USED : 3	MAXIMUM NUMBER OF ITERATIONS		
	ACTUAL NUMBER OF BUSES : 3	: 15		
	NUMBER OF 2 WIND. TRANSFORMERS: 0 NUMBER OF 3 WIND. TRANSFORMERS	BUS VOLTAGE BELOW WHICH LOAD MODEL IS CHANGED : 0.75000		
	: 0	CIRCUIT BREAKER RESISTANCE (PU)		
	NUMBER OF TRANSMISSION LINES : 3 NUMBER OF SERIES REACTORS : 0	: 0.00000 CIRCUIT BREAKER REACTANCE (PU)		
	NUMBER OF SERIES CAPACITORS : 0	: 0.00010		
	NUMBER OF CIRCUIT BREAKERS : 0	TRANSFORMER R/X RATIO :		
	NUMBER OF SHUNT REACTORS : 0 NUMBER OF SHUNT CAPACITORS : 0	0.05000		
	NUMBER OF SHUNT IMPEDANCES : 0			
	NUMBER OF GENERATORS : 2	ANNUAL PERCENTAGE INTEREST		
	NUMBER OF LOADS : 2 NUMBER OF LOAD CHARACTERISTICS :	CHARGES : 15.000 ANNUAL PERCENT OPERATION &		
	0 NUMBER OF UNDER FREQUENCY	MAINTENANCE CHARGES: 4.000		
	RELAY: 0NUMBER OF GEN CAPABILITY CURVES: 0 NUMBER OF FILTERS	LIFE OF EQUIPMENT IN YEARS : 20.000		
	: 0	ENERGY UNIT CHARGE (KWHOUR)		
	NUMBER OF TIE LINE SCHEDULES : 0 NUMBER OF CONVERTORS : 0	: 2.500 Rs LOSS LOAD FACTOR :		
	NUMBER OF CONVERTORS : 0 NUMBER OF DC LINKS : 0	0.300		
	NUMBER OF SHUNT CONNECTED FACTS:	COST PER MVAR IN LAKHS :		
	0 POWER FORCED LINES : 0	5.000 Rs		
	TOWER TORCED EINES . 0			
	NUMBER OF TCSC CONNECTED : 0 NUMBER OF SPS CONNECTED : 0	ZONE BLOAD OLOAD REEN OCEN		
	NUMBER OF SPS CONNECTED : 0  NUMBER OF UPFC CONNECTED : 0	ZONE PLOAD QLOAD PGEN QGEN SHREACT SHCAP CLOAD		
		0 1.000 1.000 1.000 1.000 1.000		
	LOAD FLOW - FAST DE-COUPLED	1.000 1.000		
	TECHNIQUE : 0	1 1.000 1.000 1.000 1.000 1.000		
	NUMBER OF ZONES : 1 PRINT OPTION : 3 -	1.000 1.000		
	BOTH DATA AND RESULTS PRINT			
	PLOT OPTION : 1 - PLOTTING WITH PU VOLTAGE	BUS DATA		
	NO FREQUENCY DEPENDENT LOAD	BUS NO. AREA ZONE BUS KV VMIN-PU		
	FLOW, CONTROL OPTION: 0	VMAX-PU NAME		
	BASE MVA : 100.000000	1 1 1 11.000 0.950 1.050 Bus1		
	100.00000	2 1 1 11.000 0.950 1.050 Bus2		

3 1 1 11.000 0.950 1.050 Bus3	0
TRANSMISSION LINE DATA	2 3 Bus3 50.000 20.000 0.000 0.000 100.000 1.000 0 0 3
STA CKT FROM FROM TO TO LINE PARAMETER RATING KMS kV NODE NAME* NODE NAME* R(P.U) X(P.U.) B/2(P.U.) MVA	TOTAL SPECIFIED MW GENERATION : 450.00000
3 1 1 Bus1 2 Bus2 0.04000 0.16006 0.15000 250 1.0 3 1 1 Bus1 3 Bus3 0.01000 0.08000 0.07000 250 1.0 3 1 2 Bus2 3 Bus3 0.03000 0.10000 0.04000 250 1.0	TOTAL MIN MVAR LIMIT OF GENERATOR: 140.00000  TOTAL MAX MVAR LIMIT OF GENERATOR: 235.83100  TOTAL SPECIFIED MW LOAD: 300.00000 reduced 300.00000  TOTAL SPECIFIED MVAR LOAD: 170.00000 reduced 170.00000  TOTAL SPECIFIED MVAR COMPENSATION: 0.00000 reduced 0.00000
TOTAL LINE CHARGING SUSCEPTANCE : 0.52000 TOTAL LINE CHARGING MVAR AT 1 PU VOLTAGE: 52.000 TOTAL CAPACITIVE SUSCEPTANCE : 0.00000 pu - 0.000 MVAR TOTAL INDUCTIVE SUSCEPTANCE : 0.00000 pu - 0.000 MVAR	TOTAL (Including out of service units) TOTAL SPECIFIED MW GENERATION : 450.00000 TOTAL MIN MVAR LIMIT OF GENERATOR: 140.00000 TOTAL MAX MVAR LIMIT OF GENERATOR: 235.83100 TOTAL SPECIFIED MW LOAD : 300.00000 reduced 300.00000 TOTAL SPECIFIED MVAR LOAD :
GENERATOR DATA  SL.NO* FROM FROM REAL Q-MIN Q-MAX V-SPEC CAP. MVA STAT NODE NAME* POWER(MW) MVAR MVAR P.U. CURV RATING	170.00000 reduced 170.00000 TOTAL SPECIFIED MVAR COMPENSATION : 0.00000 reduced 0.00000  GENERATOR DATA FOR FREQUENCY DEPENDENT LOAD FLOW
1 1 Busl 250.0000 70.0000 165.8310 1.0000 0 300.00 3 2 2 Busl 200.0000 70.0000 70.0000 1.0000 0 250.00 3	SLNO* FROM FROM P-RATE P-MIN P-MAX %DROOP PARTICI BIAS NODE NAME* MW MW MW FACTOR SETTING C0 C1 C2
LOAD DATA  SLNO FROM FROM REAL REACTIVE COMP COMPENSATING MVAR VALUE CHAR F/V  * NODE NAME* MW MVAR MVAR MIN MAX STEP NO NO	1 1 Busl 250.000 0.0000 250.0000 4.0000 0.0000 0.0000 100.0000 2 2 Busl 200.000 0.0000 200.0000 4.0000 0.0000 0.0000
STAT	0.0000
1 2 Bus2 250.000 150.000 0.000 0.000 100.000 1.000 0 0	Slack bus angle (degrees): 0.00

TOTAL NUMBER OF ISLANDS IN THE LINE FLOWS AND LINE LOSSES GIVEN SYSTEM : 1 TOTAL NUMBER OF ISLANDS HAVING SLNO CS FROM FROM то то ATLEAST ONE GENERATOR: 1 FORWARD LOSS SLACK BUSES CONSIDERED FOR THE NODE NAME NODE NAME MW STUDY MVAR MW MVAR LOADING ISLAND NO. SLACK BUS NAME SPECIFIED MW 1 1 1 Bus1 2 Bus2 39.327 24.288 1 1 Bus1 250.000 1.2360 -22.8217 26.3^ 2 1 1 Bus1 3 Bus3 62.867 38.401 0.6014 -8.6200 32.6^ 3 1 2 Bus2 3 Bus3 -11.921 -32.935 0.3574 -5.8880 15.2& ITERATION MAX P BUS MAX P MAX Q BUS MAX Q COUNT NUMBER PER UNIT ! NUMBER OF LINES LOADED BEYOND NUMBER PER UNIT 125% : 0 @ NUMBER OF LINES LOADED BETWEEN 1 2 0.500 3 0.149 100% AND 125%: 0 2 2 0.055 3 0.006 # NUMBER OF LINES LOADED BETWEEN 3 2 0.004 0.0003 75% AND 100%: 0 4 2 0.0003 0.000 \$ NUMBER OF LINES LOADED BETWEEN 5 2 0.0002 0.822 50% AND 75%: 0 6 2 0.170 3 0.029 ^ NUMBER OF LINES LOADED BETWEEN 7 2 0.019 3 0.003 25% AND 50%: 2 

 2
 0.001
 2
 0.000

 3
 0.000
 2
 0.000

 8 & NUMBER OF LINES LOADED BETWEEN 9 1% AND 25%: 1 Number of p iterations: 6 and Number of q \* NUMBER OF LINES LOADED BETWEEN iterations: 7 0% AND 1%: 0 ISLAND FREQUENCY SLACK-BUS **BUS VOLTAGES AND POWERS** CONVERGED(1) V-MAG ANGLE NODE FROM MW1 50.00000 1 0 MVAR MW MVAR MVAR P.U. DEGREE NO. NAME GEN -----GEN LOAD LOAD COMP ---- ------ ----- ----- ------ ------Summary of results TOTAL REAL POWER GENERATION: 1 Bus1 1.0000 0.00 102.194 62.689 302.194 MW 0.000 0.000 0.000 < TOTAL REAL POWER INJECT,-ve L: 2 Bus2 0.9226 -2.93 200.000 70.000 0.000 MW250.000 150.000 0.000 @ TOTAL REACT. POWER GENERATION: 3 Bus3 0.9585 -2.74 0.000 0.000 132.689 MVAR 50.000 20.000 0.000 GENERATION pf : 0.916 TOTAL SHUNT REACTOR INJECTION: -NUMBER OF BUSES EXCEEDING  $0.000 \, MW$ MINIMUM VOLTAGE LIMIT (@ mark): 1 TOTAL SHUNT REACTOR INJECTION: NUMBER OF BUSES EXCEEDING  $0.000~\mathrm{MVAR}$ MAXIMUM VOLTAGE LIMIT (# mark): 0 NUMBER OF GENERATORS EXCEEDING TOTAL SHUNT CAPACIT.INJECTION: MINIMUM Q LIMIT (< mark) : 1  $0.000 \, MW$ NUMBER OF GENERATORS EXCEEDING TOTAL SHUNT CAPACIT.INJECTION: MAXIMUM Q LIMIT (> mark) : 0 0.000 MVAR

MVAR generation 132.6894

MVAR - capacitive 0.0000

MW loss

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TOTAL TCSC REACTIVE DRAWL	:	
0.000 MVAR		1

TOTAL SPS REACTIVE DRAWL Area wise distribution 0.000 MVAR Description Area # 1

TOTAL UPFC FACTS. INJECTION MW generation 302.1941

0.0000 MVAR

TOTAL SHUNT FACTS.INJECTION

MW load 300.0000 0.000 MVAR TOTAL SHUNT FACTS.DRAWAL

0.000 MVAR MVAR load 170,0000

TOTAL REAL POWER LOAD : 300.000 MVAR compensation 0.0000

MW TOTAL REAL POWER DRAWAL -ve g:

0.000 MW

TOTAL REACTIVE POWER LOAD

**MVAR** loss -37.3297 170.000 MVAR

LOAD pf 0.870

MVAR - inductive 0.0000 TOTAL COMPENSATION AT LOADS

0.000 MVAR

TOTAL HVDC REACTIVE POWER 0.000 MVAR

TOTAL REAL POWER LOSS (AC+DC) : 2.194845 MW ( 2.194845+ 0.000000) Date and Time: Fri Oct 17 12:23:30 2014

PERCENTAGE REAL LOSS (AC+DC) : \_\_\_\_\_

0.726

TOTAL REACTIVE POWER LOSS 37.329685 MVAR

Zone wise distribution Description Zone # 1

MW generation 302.1941

MVAR generation 132.6894

MW load 300.0000

MVAR load 170.0000

MVAR compensation 0.0000

MW loss 2.1948

MVAR loss -37.3297

MVAR - inductive 0.0000

MVAR - capacitive 0.0000

Zone wise export(+ve)/import(-ve)

Zone # 1 MW & MVAR

#### OUTPUT RESULT OF LOAD FLOW VI. **ANALYSIS**

2.1948

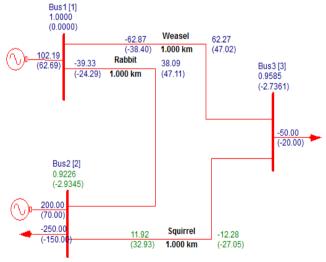


Figure-3 Output Result of Load Flow Analysis

#### VII. CONCLUSION

Power flow or load-flow studies are important for planning future expansion of power systems as well as in determining the best operation of existing systems. The principal information obtained from the power flow study is the magnitude and phase angle of the voltage at each bus, and the real and reactive power flowing in each line. In this paper, Gauss-Siedel method is used for analyzing the load flow of the IEEE-3 bus systems. This is verified by using the guass-seidel method and Mipower for 3 bus system. This Mipower software can be applicable for any number of buses. The standard IEEE 3 bus input data is used for IEEE 3 bus system .The future scope for this project can be extended with Newton-Raphson method and Fast Decoupled methods.

#### REFERENCES

- [1] Ray D. Zimmerman and Hsiao-Dong Chiang." Fast Decoupled Power Flow for Unbalanced Radial Distribution Systems" 1995IEEE.pp241-250.
- [2] P. S. Bhowmik, D. V. Rajan, and S. P. Bose "Load Flow Analysis: An Overview" World Academy of Science, Engineering and Technology 63 2012.
- [3] Dharamjit and D.K.Tanti "Load Flow Analysis on IEEE 30 bus System " International Journal of Scientific and Research Publications.Vol.2,Issue 11, Nov. 2012.
- [4] Nagrath & Kothari, "Morden power system analysis", Tata McGraw Hill, June 2006. pp (177, 186,, 205,217).
- [5] H. H. Happ, "Optimal power dispatch-A comprehensive survey", IEEE Trans. Power Apparat. Syst.,vol. PAS-90, pp. 841-854, 1977.
- [6] IEEE working group, "Description and bibliography of major economic-security functions part-II and III, IEEE Trans. Power Apparat. Syst., vol.PAS-100,pp. 215-235, 1981.
- [7] J. Carpentier, "Optimal power flow, uses,methods and development", Planning andoperation of electrical energy system Proc. Of IFAC symposium, Brazil, 1985, pp. 11-21.
- [8] B. H. Chowdhury and Rahman, "Recent advances in economic dispatch", IEEE Trans. Power Syst., no.5, pp.1248-1259, 1990.
- [9] S. D. Chen and J. F. Chen, "A new algorithm based on the Newton-Raphson approach for real-time emission dispatch", Electric Power Syst. Research, vol.40,pp. 137-141,1997.
- [10] J. A. Momoh, "A generalized quadratic-based model for optimal power flow", CH2809-2/89/0000-0261,\$1.00©1989IEEE, pp. 261-267.
- [11] X. Lin, A. K. David and C. W. Yu, "Reactive power optimization with voltage stability consideration in power market systems",IEEE proc.-Gener. Transm. Distrib., vol.150, no.3,pp. 305-310,May2003
- [12] Glenn W Stagg, and I.Stagg, "Computer Methods in Power System Analysis".
- [13] J W.D. Stevenson Jr., "Elements of power system analysis", (McGraw-Hill, 4th edition, 1982).
- [14] H. Dommel, "Digital methods for power system analysis" (in German), *Arch. Elektrotech.*, vol. 48, pp. 41-68, February 1963 and pp. 118-132, April 1963.
- [15] Carpentier "Optimal Power Flows", *Electrical Power and Energy Systems*, Vol.1, April 1979, pp 959-972.