

Landing Gear Stress Analysis During Rough Landing

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Abstract:- Landing gear is the undercarriage of an aircraft or spacecraft, and is used in both take-off and landing. The landing gear shock absorber is an integral component of an aircraft's landing gear. The role of the shock absorber is to absorb and dissipate energy upon impact, such that the forces imposed on the aircraft's frame are tolerable. The shock absorber may be an independent element, or integrated with the landing gear strut. The aircraft may tend to land in a smooth manner or even in a rough manner. The landing gear components must be able to withstand the entire force.

The aim of this paper is to develop a landing gear which is suitable for rough landing too. This is achieved by creating a 3-D model of the Landing gear in CATIA V5 software and subject it to ANSYS to determine the variation in the displacement and Von miss stress behaviour for three materials (steel, Aluminium, Titanium) which is subjected to static loading and plot the results for same loading condition and suggest the suitable material. And then the landing gear is modelled and the modelled component is analysed using ANSYS Software to study its structural performance thereby replacing the material of the landing gear.

Keywords:- Landing gear, Shock absorber, Loads, CATIA V5, ANSYS, Von miss stress

I. INTRODUCTION

An aircraft landing gear shock absorber is a combination of mechanical structure, pneumatics and hydraulic damping used for transmitting impact loads. This project focuses energy based modelling of the shock absorber. A landing gear shock absorber model includes an aircraft mass with

wing lift, shock absorber piston and cylinder structure, three hydraulic chambers representing the air chamber, hydraulic chamber, and rebound chamber, and tire. The design objective is to minimize ground reaction loads. The key design variables are centred on fixed or variable orifice definitions. [1]

II. THE DESIGN DECISION SITUATION

A. System Description

This paper is aimed at design problem. It is centred in the hydro-mechanical domain. [2]. The majority of landing gear shock struts are comprised of a piston and cylinder, pressurized by compressed nitrogen, using hydraulic fluid as the damping medium. The hydraulic chamber is normally separated from the air chamber by an orifice. This orifice may be fixed, or vary with stroke (that is, travel of the piston) or vary with pressure. Other arrangements are often employed, including dividing the air chamber into a low and high pressure volume to provide more complex (and tailor able) compression characteristics. An aircraft is supported entirely on air springs. Compression

characteristics of the gas produce a pronounced nonlinear spring rate, the slow, isothermal compression curve. During rapid stroking of the shock, hydraulic pressure due to viscous damping across the orifice becomes dominate, giving the strut the ability to react large dynamic loads. Often a second orifice and hydraulic chamber is used to meter the stroke velocity in the opposite (extending) direction.

B. The Design Decision

First step in design process is to decide about internal chamber arrangement and overall size of the piston/cylinder combination, followed by deciding pressure settings and damping characteristics. An efficient landing gear design balances the size and complexity of the landing gear with the load attenuation ability of the gear. This project will consider only a single landing gear, not a full aircraft. As such, aerodynamic effects, and body pitch and roll will not be explored. Also, other landing gear functions such as steering, braking, and retraction/extension for stowage will not be considered, other than how they may affect the mass of the components. [3].

III. DEVELOPMENT

The overall fundamental objective is to maximize the landing gear performance. It is basically divided into four fundamental objectives. [4]. The focus is on the energy absorption performance aspects

- a) Minimize Landing Loads
- b) Minimize Taxi Loads
- c) Minimize Shock Absorber Volume, $L \times \pi D^2/4$
- d) Maximize Composite Reliability and Maintainability

IV. SIMULATION

A. Model Requirements

- 1) "Fixed inputs" are those intend to code into the model to represent physical features, but do not intend to explore for design. [5].

These include:

- i) Tire characteristics (stiffness, stroke length),
- ii) Fluid characteristics (hydraulic oil)

- 2) "Design variables" are parameters (varied in comparative analysis).

These are:

- i) Stroke length, S, cm
- ii) Piston diameter, D, cm
- iii) Shock pressure, P, kPa
- iv) Shock volume, further divided into air volume, Va, and fluid volume, Vf, cm³

v) Orifice characteristics, (units tbd)
 3) "Variation variables" will be used to explore randomness or uncertainty in the model:

- i) Friction (piston to cylinder)
 - ii) Gas compression characteristics (real gas or ideal gas).
- 4) "Usage variables" are parameters (varied to exercise the model in realistic usage scenarios).

These will include:

- i) Aircraft mass: Only a proportional amount of mass will be applied to the mode
- ii) Aircraft forward speed, m/sec
- iii) Vertical speed (landing cases only), m/sec
- iv) Bump profile (height as a function of distance).

B. Assumptions and Simplifications

- 1) Model rigid structure for the piston and cylinder, neglecting bending and expansion under load
- 2) Will model a single strut with 1-D motion
- 3) Neglect gas-fluid mixing
- 4) Assume constant fluid properties
- 5) Neglect high frequency dynamic behaviour.

V. LANDING GEAR DESIGN

The Landing Gear was modelled with standard dimensions derived from various literature surveys. By using that dimensions, the parts of Landing Gear was modelled. After all individual part creation, assembly of all parts is done to create a single component. The assembled model of the landing gear is shown in fig.1. The three view diagram and isometric diagram of the model is shown.

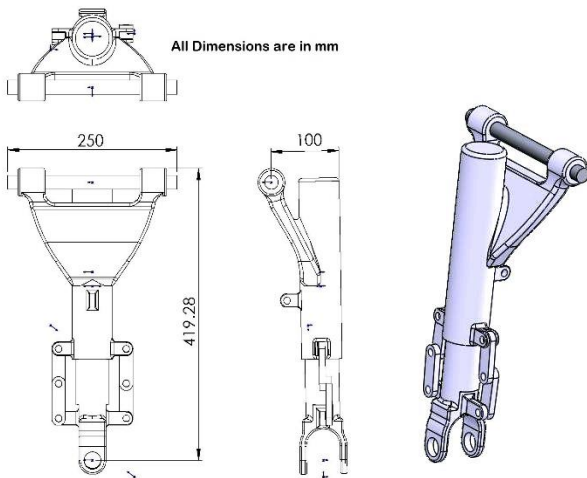


Fig.1: Assmblled model of Landing gear

VI. NUMERICAL ANALYSIS

A. FEA:

Finite Element Analysis (FEA) uses numerical methods and algorithms to solve and analyse problems that involve analysis of structures or objects using computers.

B. Outline Finite Element Analysis Process

The three basic elements are

- i) Pre-processor ,
- ii) Solver ,
- iii) Post-Processor

C. Material Selection

In general the landing gear is made of metal substrate which is a Titanium alloy Ti-6 Al – 4V. The SAE 1035 steel and 7075-76 aluminium alloy is replaced to improve the structural behaviour of the Landing Gear assembly. [6]. The properties of these materials are listed in below Table:1.

Table: 1
 Material property

Property	Ti-6 Al – 4V Titanium Alloy	SAE 1035 Steel	7075-76 Aluminium alloy
Density	7.87 g/cm ³	4.43 g/cm ³	2.81 g/cm ³
Young's Modulus	196 GPa	113.8 GPa	71.7 GPa
Coefficient of Thermal Expansion	11.9 μC ⁻¹	8.6 μC ⁻¹	23.6 μC ⁻¹
Reference Temperature	20°C	20°C	20°C
Poisson's Ratio	0.29	0.342	0.33
Tensile Yield Strength	550 MPa	880 MPa	503 MPa
Tensile Ultimate Strength	620 MPa	950 MPa	572 MPa

D. Geometry Creation

In this process, geometry for the Landing Gear assembly is created. The Landing Gear and its components are modelled earlier which is now a 3D model. The Landing Gear assembly has to be imported as an IGS file format to get a proper structure. The imported Landing Gear assembly model is as shown in figure.2.

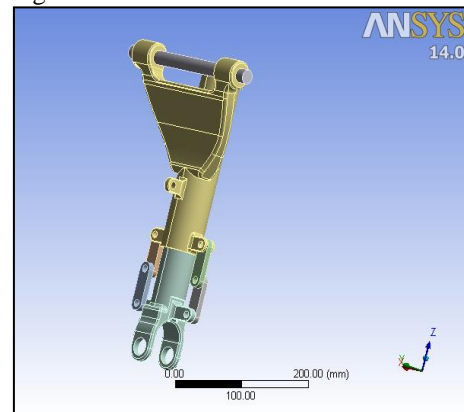


Fig.2: Piston assembly

E. Meshing

Different meshing characteristics were used for the domain. In the simulations, the piston component surfaces were discretized with triangular mesh elements.

F. Boundary Condition

The problem is a structural analysis problem. The boundary condition for the problem is Force of 10 KN with the arm to be fixed.

G. Numerical Results

The structural behaviour of the Landing Gear has been studied for the above mentioned boundary conditions. The results obtained by these are shown in below. The Table. II shows the structural behaviour of the Landing Gear assembly. From the table it's clear that the SAE 1035 Steel material holds a very

good structural property. The stress concentration over the SAE 1035 Steel is more than the Titanium alloy 6Al-4V and 7075-76 Aluminium alloy.

Table: 2
 Structural Behavior

Loading Condition @ 10000 N	Deformation(m m)	Stress(Mpa)	Strain
Titanium alloy 6Al-4V	1.7734	232.03	0.00211
7075-76 Aluminum alloy	2.8162	232.7	0.00336
SAE 1035 Steel	1.0318	235.05	0.00125

From figure 3, 4, and 5, the values of deformation for three cases were observed. The deformation contour clearly shows that the deformation is high for the aluminium alloy when compared to other two materials. The SAE 1035 holds a less deformation even blow that of titanium. So in terms of deformation the SAE 1035 holds a better performance than the other two materials.

VII. SIMULATION OUTCOMES

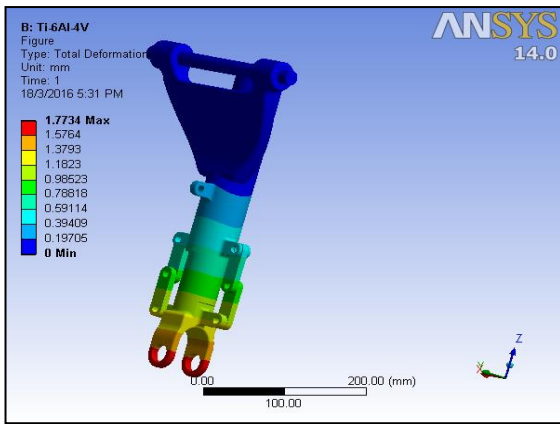


Fig.3: Deformation for case-1

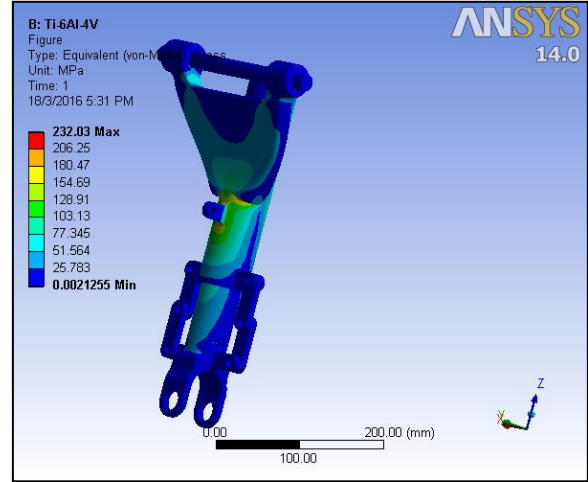


Fig.6: Stress for case-1

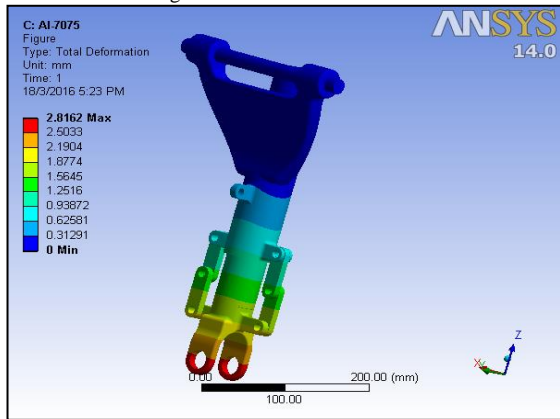


Fig.4: Deformation for case-2

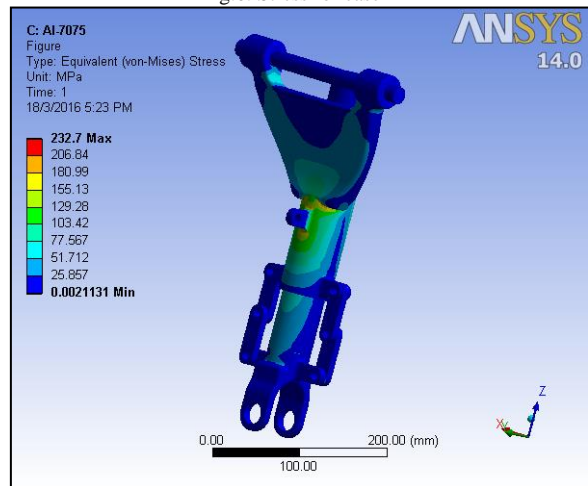


Figure.7 Stress for case-2

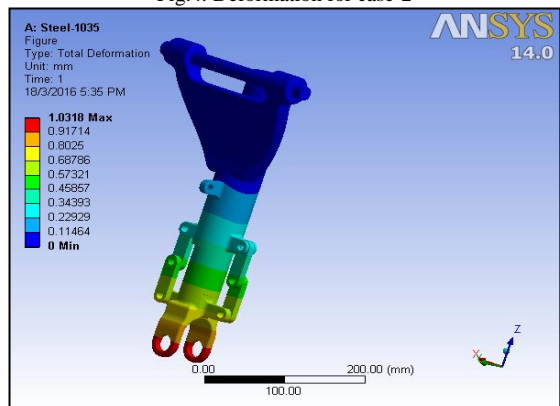


Figure.5: Deformation for case-3

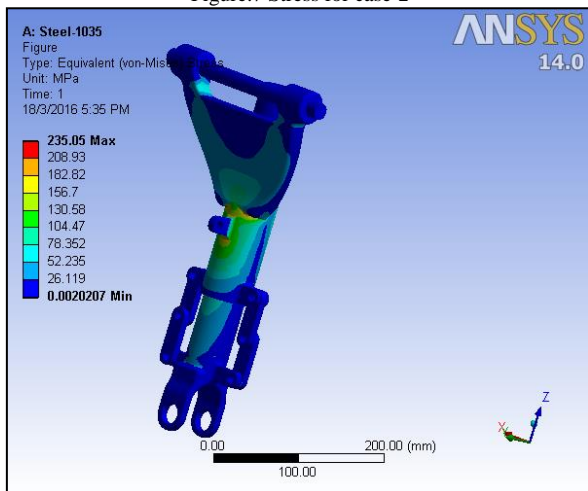


Figure.8 Stress for case-3

From figures 6, 7 and 8, the value of stresses are determined. The stress concentration over the SAE 1035 is higher than the other cases. The SAE 1035 holds a higher yield value than the other materials. So the higher stress doesn't affect the SAE 1035, so in terms of stress concentration over the model it's recommended to us SAE 1035 material.

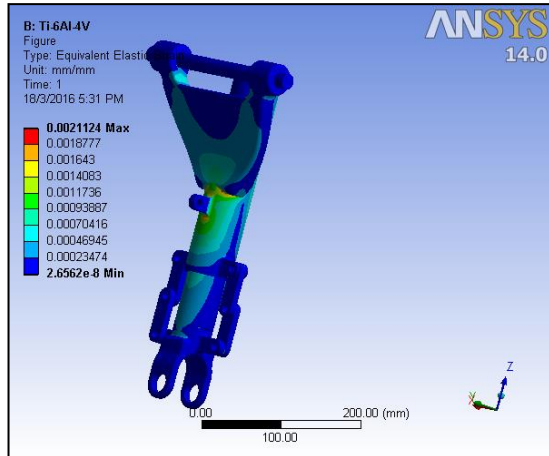


Fig.9: Strain for case-1

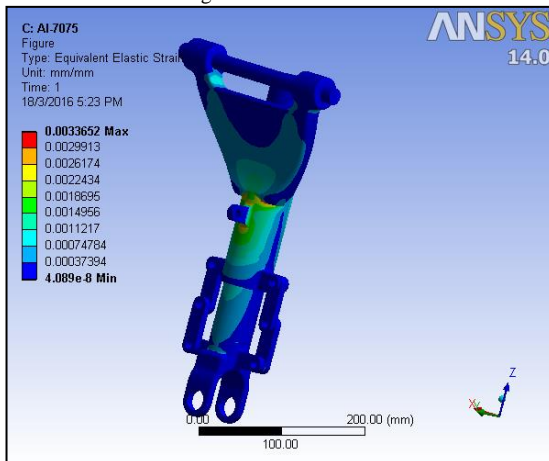


Fig.10 Strain for case-2

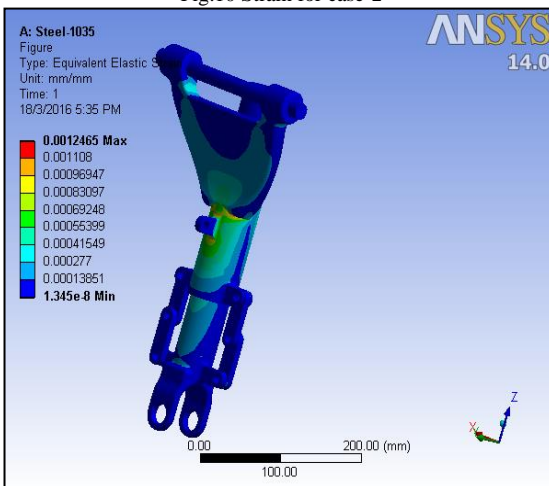


Fig.11: Strain for case-3

From figures 9, 10 and 11, the value of strain are observed. Since the stress is directly proportional to strain the performance of the strain also will be better for the SAE 1035 material. So in terms of all structural parameters the SAE 1035 material holds a good performance.

VIII. CONCLUSION

The landing gear is modelled and assembled using SOLIDWORKS. The assembled CAD model has been considered to perform structural analysis by finite element approach using the ANSYS package. In general the accuracy of the solution depends on the mesh quality. Each component has been checked for its mesh quality to ensure the solution accuracy. Also before the meshing process model has been simplified. After these processes the structural analysis has been carried for the landing gear assembly for three different materials Titanium alloy 6A1-4V, 7075-76 Aluminium alloy and SAE 1035 Steel. The results show that the SAE 1035 steel holds a good performance when compared to other materials. The result has been compared on the basis of the parameters like deformation, stress and strain. The SAE 1035 steel has a less deformation when compared to other materials; around 35 % of the deformation has been reduced when compared. So the implementation of this material would help to avoid the landing gear damage and also it can have a better life than the other materials due to its less damage.

IX. REFERENCE

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