



established, massive CO<sub>2</sub> emission is a threat to the earth environment due to its propensity to cause global warming. The intervention method that can be adopted indeed, is CO<sub>2</sub> sequestration. There is therefore the need for a combination of CO<sub>2</sub>-EOR and permanent CO<sub>2</sub> storage operations along the region to control the forecasted menace and provide a means for the sub region to contribute solutions to the release of greenhouse gases.

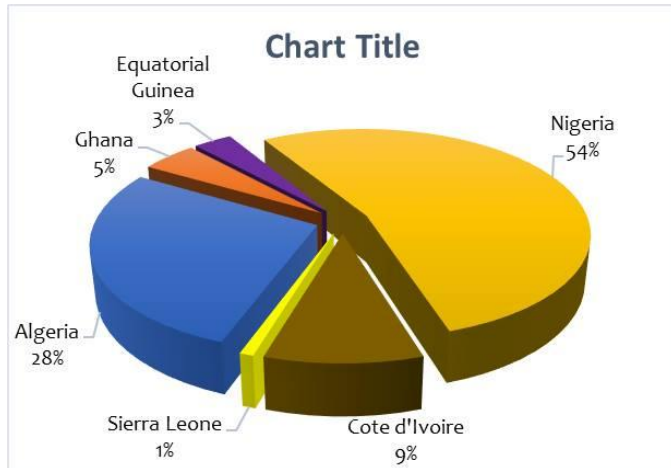


Fig. 2. West Africa's contribution to CO<sub>2</sub> emissions [5]

### B. Overview of CCS

Sequestering atmospheric CO<sub>2</sub> released from industrial sources such as petroleum extractive plants involve capturing and transporting CO<sub>2</sub> through pipelines systems to the injection site, compressing CO<sub>2</sub> to achieve the injection pressure, and injecting it into the reservoir [6]. The capture process and method (as shown in Figure 3), the processing, transport and injection methods are well-established technologies that have had excellent safety records in CCS operations. The element of uncertainty has to do with the integrity of CO<sub>2</sub> trapping after injection, which has not yet been fully understood because the subsurface region (SSR) in itself is only partly understood and often processes involving the SSR are described by means of correlated data and information from analogous geological structures. It is imperative therefore to properly assess geological formations before they are sanctioned for long term CO<sub>2</sub> storage. Hydrocarbon bearing reservoirs are appealing as save storage sites since they are best understood to have geologic seals that successfully trap buoyant reservoir fluids for millions of years [6].

The International Energy Agency (IEA) report on Carbon Capture and Storage [7] identifies that highly prospective geological basins for CO<sub>2</sub> storage are mainly found in the United States and Canada, Siberia, the Middle East, and North and West Africa within existing oil and gas regions. The report indicates that in Africa the CO<sub>2</sub> storage capacity in aquifers varies from 6 to 220 Gt and in oil and gas fields from 30 to 280 Gt (Figure 4). North and West Africa were reported to have the highest potential for CO<sub>2</sub> storage in oil and gas fields.

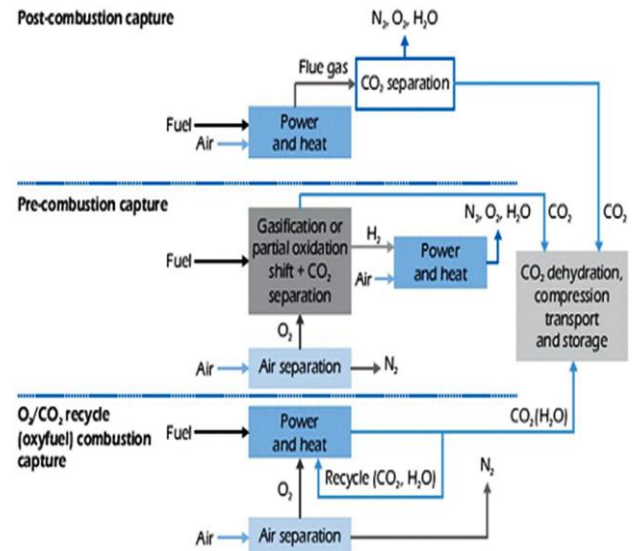


Fig. 3. CO<sub>2</sub> capture process [7]

The trapping of CO<sub>2</sub> can occur in one of three ways elaborated below;

- Physical trapping: These can take two main forms: static trapping where upwards movement of CO<sub>2</sub> is blocked by impermeable layer of shale or clay rock, also called a “cap rock”, and residual-gas trapping in a porous structure provided by capillary forces.
- Chemical trapping: This occurs by dissolution or by ionic trapping. Once dissolved, the CO<sub>2</sub> reacts chemically with minerals in the geological formation (mineral trapping) or adsorbs on the mineral surface (adsorption trapping).
- Hydrodynamic trapping: The CO<sub>2</sub> migrates upward at a very low velocity and is being trapped in intermediate layers. Large quantities of CO<sub>2</sub> could be stored using this mechanism, since the migration to the surface would take millions of years.

### C. Overview of CO<sub>2</sub>-EOR

Oil recovery techniques have traditionally been grouped into three categories, based on when they are likely to be implemented in a typical oilfield. Primary, Secondary and Tertiary recovery methods. The successive use of primary recovery and secondary recovery in an oil reservoir produces about 15% to 40% of the original oil in place, depending on the properties of oil and the characteristics of the reservoir rock. Tertiary oil recovery methods aim at altering the flow properties of crude oil and the rock-fluid interactions in the reservoir to improve oil flow; one of these techniques is CO<sub>2</sub>-EOR. The term ‘tertiary oil recovery’ has recently been disfavored in the literature and substituted by the term enhanced oil recovery or EOR [8].

CO<sub>2</sub>-EOR is an enhanced oil recovery method in which carbon dioxide (CO<sub>2</sub>) is injected into a reservoir to increase production by reducing oil viscosity and providing miscible or partially miscible displacement of the oil. The applicability of the two main processes developed for CO<sub>2</sub> flooding (miscible and immiscible displacement) will depend on the reservoir conditions. The process, moreover, can also be distinguished based on the type of CO<sub>2</sub> injection method implemented. Here, we discriminate between the Water Alternating Gas (WAG) method and the Gravity Stable Gas Injection (GSGI) method. WAG has an advantage over GSGI in that it can be performed on a small scale; while in general, GSGI is applied in the whole oilfield. Hence GSGI projects are likely to recover more oil and store larger CO<sub>2</sub> volumes [9]. A schematic of the miscible CO<sub>2</sub>-EOR operation is shown in Figure 5.

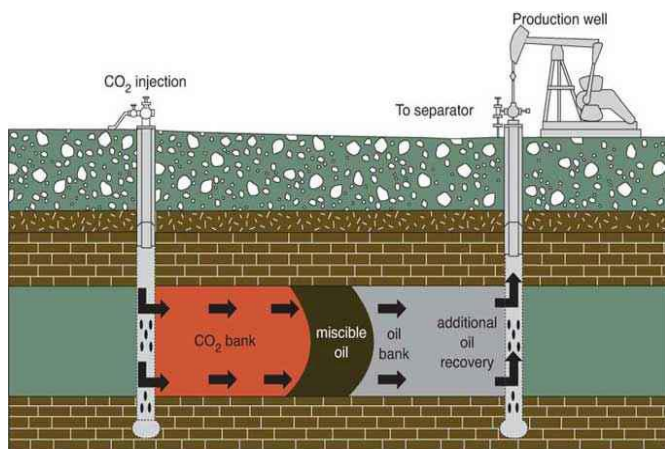


Fig. 5. schematic of the miscible CO<sub>2</sub>-EOR operation [10]

EOR by CO<sub>2</sub> is a method that is widely applied in recovery techniques around the world and provides a unique opportunity to gain a considerable financial return for storing anthropogenic CO<sub>2</sub> once oil production declines prior to field abandonment. The relationship between CO<sub>2</sub> storage and CO<sub>2</sub>-EOR is important and unique because while the CO<sub>2</sub> serves as an agent for maximizing recovery, the entire EOR operation, in turn, also stores the greenhouse gas away from the Earth's atmosphere by keeping it locked in the geological reservoir formations.

## II. METHODOLOGY

Along the WATM there are several oil and gas fields. In this study, the oil fields that were considered are Jubilee field – Ghana; Agbami field – Nigeria; Zafiro Complex – Equatorial Guinea; Baobab – Cote d'Ivoire, the Espoir field - Cote d'Ivoire, Girassol Complex – Angola. The fields were selected to cover the regional margin under study and partly based on available data

### A. Screening of reservoirs suitable for CO<sub>2</sub>-EOR

To merge CCS with oil recovery would first require investigating for field suitability for CO<sub>2</sub>-EOR. Theoretically, any type of reservoir formation; carbonate or sandstone, could be suitable for CO<sub>2</sub>-EOR but for various technical and economic reasons, not all reservoirs would be good candidate for CO<sub>2</sub>-EOR. Several reservoir properties are considered. Broadly speaking, oil viscosity, oil API-gravity, reservoir depth, reservoir oil saturation and reservoir heterogeneity are

among the most important [11]. The most critical parameter is the Minimum Miscibility Pressure (MMP) for each reservoir. The MMP is defined as the minimum pressure at which the injected CO<sub>2</sub> will begin to mix with the residual oil in all proportions without the existence of an interface between the fluids. The MMP is a function of oil properties, reservoir temperature, reservoir pressure and the purity of the injected CO<sub>2</sub> [11]. Therefore, it is not an easy parameter to estimate, even with full reservoir data. Due to challenges with obtaining key reservoir data on the fields along the WATM from the operators, we used a two-step approach to estimate the MMP's of the reservoirs. An oilfield was regarded as a successful candidate for CO<sub>2</sub>-EOR if the MMP was less than the initial pressure.

### B. Estimating MMP

A relationship published by Holm and Josendahl (1982) [12] and extended by Mungan (1981) [10], which estimates MMP from molecular weight of the C<sub>5+</sub> components of reservoir oil and reservoir temperature (figure 7) was used. First, the molecular weight of carbon fractions in the range greater than or equal to five (C<sub>5+</sub> components) of the reservoir oil was determined using the correlation between oil API-gravity and C<sub>5+</sub> oil molecular weight published by Lasater (1958) [13] in figure 6. The correlated data can be empirically determined by using equation 1.

$$MW = (7864.9/G)^{1/1.0386} \quad (1)$$

Where MW = C<sub>5+</sub> molecular weight and G = API oil gravity  
 The MMP estimation using the extended work of Mungan (1981) [10] was also based on equation 2, derived by using non-linear multiple regression.

$$MMP = -329.558 + (7.727 * MW * 1.005^T) - (4.377 * MW) \quad (2)$$

Where T = Temperature (°F)

These equations were used because they are simple yet accurate, and do not require too much information of the reservoir to estimate the MMP. Fields for which the temperature was not available were estimated using depth correlation with geothermal gradients.

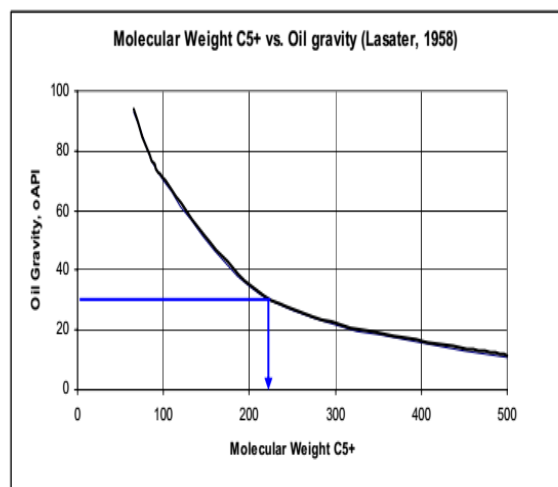


Fig. 6. Correlation between oil gravity and MW of C<sub>5+</sub> components [11]

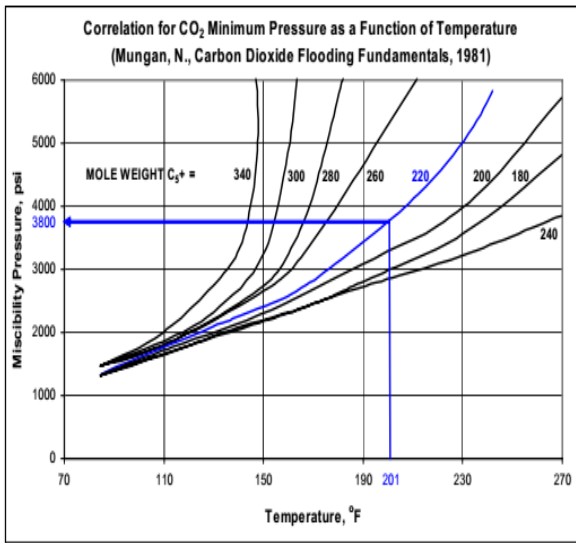


Fig. 7. Nonlinear relationship between temperature, C5+ MW of components and MMP [11]

**C. Screening and Assessment of Reservoirs Suitable for CO<sub>2</sub>-EOR and CO<sub>2</sub> storage**

A critical issue for geological storage of CO<sub>2</sub> is ensuring that the stored CO<sub>2</sub> does not escape from the host reservoir formation. To ensure a robust screening system for the proposed reservoirs along the WATM, we adopted the method published by Shaw and Bachu [14]. It is based on the premise that an oilfield is qualified for CO<sub>2</sub> storage if the geological make-up of the reservoir fulfils some specific required indexes. Further work done by Zeng et. al (2005) [15] also proposed that the main features of assessment of CO<sub>2</sub> storage potential in oil reservoirs included reservoir properties such as depth, permeability, porosity, in-situ temperature, original pressure, trap integrity and inherent fault structures. Suitable formations should have a thick and extensive seal, be sufficiently permeable to permit injection of CO<sub>2</sub> at high flow rates without requiring overly high pressure, have sufficient porosity for large volumes of CO<sub>2</sub> to be stored, and be deeper than 800m. At this depth, CO<sub>2</sub> is most likely in a liquid or supercritical state. Under these conditions, the density of CO<sub>2</sub> is close to density of crude oils, reducing the buoyant forces that tend to drive CO<sub>2</sub> upwards (figure 8)

Per the reservoir conditions of the fields along the WATM thus, the operational screening criterion is made based on the work presented by Zeng et. al. [15]

**D. Calculation of Storage Capacity**

Based on the evidence that a reservoir is qualified for CO<sub>2</sub>-EOR, we adopted a simple volumetric formula to determine the volumetric capacity of the reservoirs to store CO<sub>2</sub>. We arrive at equation 3 by assuming that an average of 10% of STOIPP for each field would be recovered using CO<sub>2</sub>-EOR and that 0.33 tonnes of CO<sub>2</sub> would be stored for each barrel of oil produced through the flooding method.

$$\text{CO}_2 \text{ storage capacity (Mt)} = (\text{STOIPP}/10) \times 0.33 \quad (3)$$

$$\text{STOIPP} = \text{OOIP}/\text{Bo} \quad (4)$$

Where STOIPP/10 = 10% of Stock Tank Oil Initially In Place in millions of barrels; OIIP = Oil Originally In Place and Bo = Oil formation volume factor.

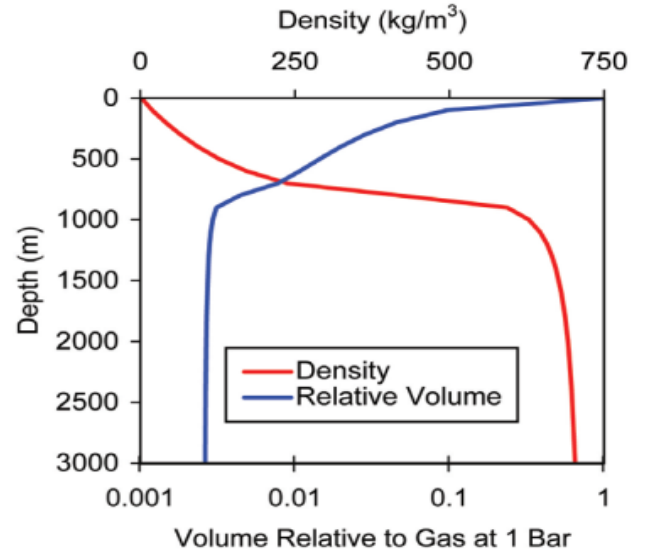
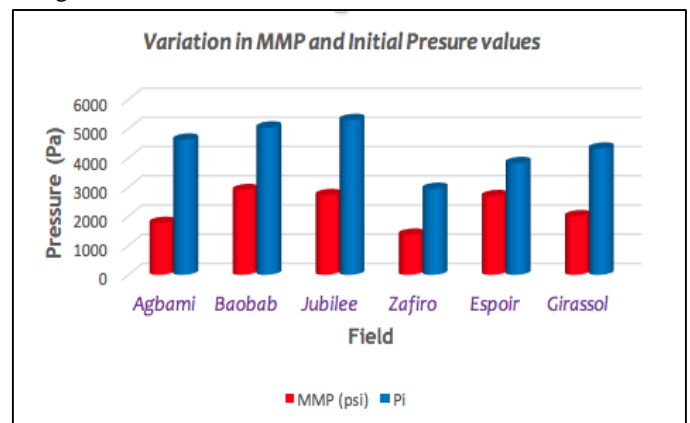


Fig. 8. Density and change in volume of CO<sub>2</sub> as a function of depth below seabed for a typical geothermal gradient [16]

Thus, by knowing the hydrocarbon volume initially in place and the formation volume factors, the CO<sub>2</sub> capacity was then calculated using excel spreadsheet.

**III. RESULTS AND DISCUSSION**

The results show clearly that all the fields investigated in this study are suitable for CO<sub>2</sub>-EOR. This provides a clear indication that these fields can be considered for CO<sub>2</sub>-EOR in the context of maximizing the economic benefit of CO<sub>2</sub> storage along the WATM in the future.



For each field scrutinized, the MMP value was way below the initial field pressure. Figure 9 shows the variation in the values for each field.

TABLE I. MW AND MMP CALCULATED VALUES FOR THE FIELDS

Field	API	MW (C5+)	T (oF)	MMP (psi)	Pi	CO <sub>2</sub> -EOR Suitability
Agbami	43	150.71	173	1771	4622	✓
Baobab	23	275.30	147	2894	5035	✓
Jubilee	37	174.17	209	2725	5295	✓
Zafiro	30	213.15	94	1370	2940	✓
Espoir	32	200.31	185	2688	3820	✓
Girassol	32	200.31	146	2000	4315	✓

The total capacity for the selected fields is approximately 369.71 Million Metric Tons (Mt). This also reflects a good storage capacity for the region and emphasizes the need for the region to consider implementation of this project (figure 10).

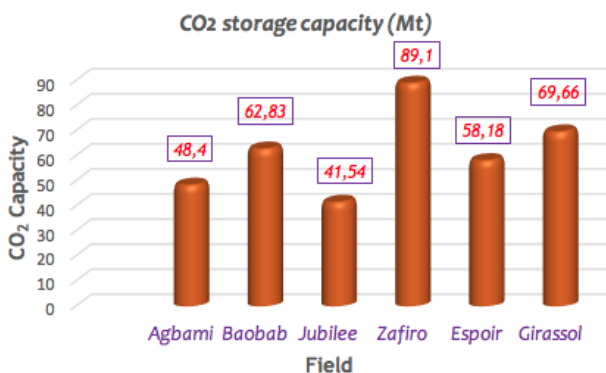


Fig. 10. Bar graph of CO<sub>2</sub> storage capacity for selected fields

Figure 11 is a schematic diagram representing a decision tree that can be used to identify CO<sub>2</sub>-EOR candidate fields along the WATM. The process used was entirely based on field geo-makeup and reservoir characteristics, and thus, only reservoir rock and fluid characteristics were considered.

#### IV. CONCLUSION AND FUTURE WORK

A high potential for increasing oil production lies along the West African Transform Margin through the implementation of CO<sub>2</sub>-EOR technique. The results indicate that this will not only increase reserves, but provide the opportunity to safely sequester anthropogenic CO<sub>2</sub> in the matured life of the fields, so the region can provide solutions to the threat of global warming. The revelations of this study calls for further studies to reveal the full potential of the west African region to successfully execute CCS.

The following recommendations are suggested;

- The screening criteria can be modified by considering other technical, engineering geoscience, and economic measures to provide industry with a full tool for field selection for CO<sub>2</sub> storage in EOR operations in the oil reservoirs along the WATM.
- Risk associated to CO<sub>2</sub> storage affects the suitability of a reservoir and consequently affects regional and national capacity estimates. It is important to conduct further work that takes risk into account as it will result in more realistic valuations of total technical CO<sub>2</sub> storage potentials along the WATM.

- Other regional considerations covering environmental, and public issues need to be investigated before full-scale implementation of CO<sub>2</sub> storage.

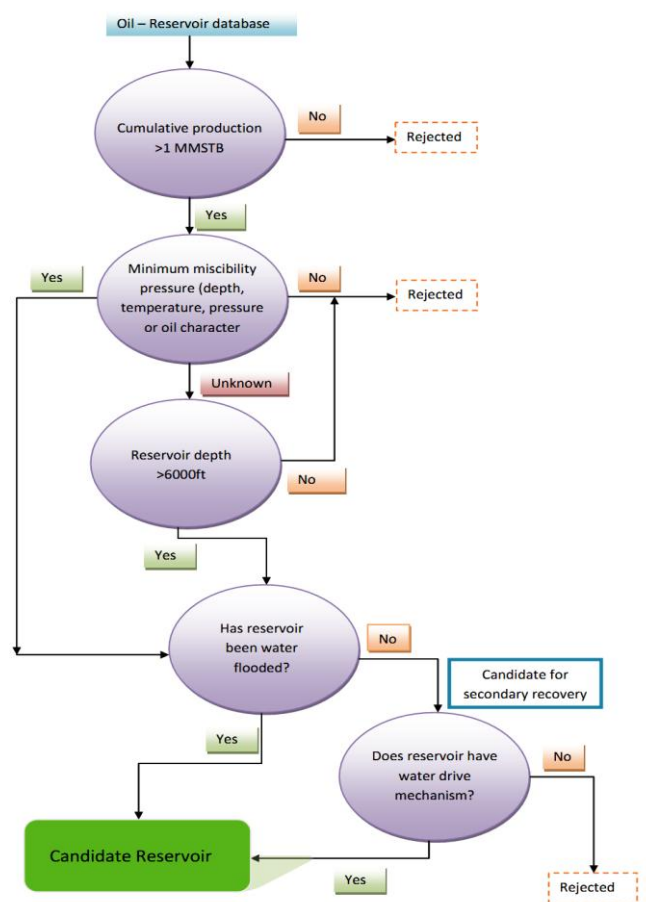


Fig. 11. Decision tree to identify CO<sub>2</sub>-EOR candidate reservoirs.

#### ACKNOWLEDGEMENTS

We gratefully acknowledge Mr. Wilberforce Aggrey Nkrumah for his supervision throughout this research work. We also appreciate Mr. Samuel Erzuah (Phd), Maame D. A. Kwajan and Stephen B. Ansah for their contributions.

---

REFERENCES

- [1] R. Verma, "Africa Programme at LSE IDEAS and PhD Candidate in the," *AAPG- Memoir*, pp. 4-5, 2008.
- [2] R. Andrea, H. Saskia, K. Leslie, W. Ton and H. Chris, "Screening CO<sub>2</sub> storage options in the Netherlands," *Science Direct*, pp. 2801-2808, 2009.
- [3] F. M. Persits, T. S. Ahlbrandt, M. L. Tuttle, R. R. Charpentier, M. E. Brownfield and K. I. Takahashi, "Map showing geology, oil and gas fields, and geologic provinces of Africa," 2002.
- [4] CDIAC, "Millennium Development Indicators," United Nations Statistics Division, 2008.
- [5] United Nations Statistics Division (UNSD), "Millennium Development Goals indicators: Carbon dioxide emissions (CO<sub>2</sub>)," 2008.
- [6] G. S. Shib, V. Namisha, A. Idar and V. P. Dimri, "Assessing the Feasibility of CO<sub>2</sub>-Enhanced Oil Recovery and Storage in Mature Oil Field: A Case Study from Cambay Basin," *Geological Society of India*, vol. 88, pp. 273-280, September 2016.
- [7] International Energy Agency, "Carbon Capture and Storage," 2008.
- [8] E. Tzimas, A. Georgakaki, C. E. Garcia and S. D. Peteves, "Enhanced Oil Recovery using Carbon Dioxide in the European Energy System," European Commission Joint Research Center, 2005.
- [9] S. Goodwear, "Subsurface Issues for CO<sub>2</sub> Flooding of UKCS Reservoirs," *ICHEME*, p. 81, 2003.
- [10] N. Mungan, "Carbon dioxide flooding fundamentals," *Journal of Canadian Petroleum Technology*, p. 87, 1981.
- [11] H. M. Holtz, N. V. Lopez and L. C. Breton, "Moving Permian Basin Technology to the Gulf Coast: the Geologic Distribution of CO<sub>2</sub> EOR Potential in Gulf Coast Reservoirs," *GCCC Digital Publication*, October 2005.
- [12] L. W. Holm and V. A. Josendal, "Effect of oil composition on miscible-type displacement by carbon dioxide," *Society of Petroleum Engineers*, pp. 87-98, 1982.
- [13] J. A. Lasater, "Bubble point pressure correlation," *Trans AIME*, p. 379, 1958.
- [14] J. C. Shaw and S. Bachu, "Screening, evaluation, and ranking of oil reservoirs suitable for CO<sub>2</sub>-flood EOR and carbon dioxide sequestration," *Journal of Canadian Petroleum Technology*, vol. 41, no. 9, pp. 51-61, 2002.
- [15] S. Zeng, X. Yang and J. Chen, "Fuzzy hierarchy analysis-based selection of oil reservoirs for gas storage and gas injection.," *Henan Petroleum*, pp. 40-46, 2005.
- [16] B. M. Sally and C. R. David, "CO<sub>2</sub> Sequestration in Deep Sedimentary Formations," *Gs Elements*, vol. 4, pp. 325-331, October 2008.