Effect of Tool geometry and Process parameters on Surface roughness and MRR in EDM of Tool Steel

Kamlesh V. Dave¹, D.S. Patel²

¹Associate Professor Mechanical department Sankal chand Patel College of Engineering Visnagar. ¹P.G Student (CAD/CAM) Mechanical Department Sankal chand Patel College of Engineering Visnagar.

ABSTRACT : Electrical discharge machining (EDM) is a nontraditional process that uses electrical spark discharge to machine electrically conducting materials such as tool and dies steels, ceramics, etc., for geometrically complex shapes, which are difficult to machine using a more traditional approach. However due to the process nature there is still failure to accurately understand process parameter influence on the surface quality, material removal rate etc. On the other hand, designing and re-shaping of required electrodes for each feature are time consuming and the number of electrode stored is very high. Therefore to increase the productivity, quality and flexibility standardized simple electrode shapes, capable to machine different features, must be analyzed. This study present the analysis based on Taguchi design and Analysis of Variance (ANOVA) we conduct experiment and find the contribution of Tool Geometry on the Surface Roughness and Material Removal Rate (MRR) with other processing parameters. And find the most significant parameter for both output parameters.

Keywords- MRR, Surface Roughness, ANOVA, Tool Geometry

1. INTRODUCTION

Electrical discharge machining (EDM) is a non-traditional machining method commonly used to produce die cavities via the erosive effect of electrical discharges. The electrically conductive tool electrode, which has the male shape of the die cavity, is prepared to machine the die cavity? The method is especially effective in machining hard die steels, complex cavities and small work pieces. Die casting, injection moulding, forging, extrusion, upset forging and power compaction dies are manufactured using EDM technology [1]

In EDM, a power supply delivers high-frequency electric pulses to the tool and the workpiece. The gap between the tool and workpiece is flushed with a stream of dielectric liquid. When an electric pulse is delivered from the power supply, the insulating property of the die electric fluid is momentarily broken down. This allows a small spark to jump the shortest distance between the tool and workpiece. A small pool of molten metal is formed on the work piece and the tool at the point of discharge. A gas bubble forms around the discharge and the molten pools. As the electric pulse ceases and the discharge disappears, the gas bubble collapses. The onrush of cool dielectric causes the molten metal to be ejected from the workpiece and the tool, leaving small craters. This action is repeated hundreds of thousands of times each second during EDM processing. This removes material from the work piece in a shape complementary to that of the tool. [2]Yan et. al. studied that Depending on the kind of material used and other requirements, positive or negative polarity can be applied. This is one of the most important parameters that affect Electrode Wear Rate, Surface Roughness, MRR[3].Pradhan et al. & Y. Lin & Sundaram et al. studied that Process modeling is an important issue to cheapen manufacturing process because it facilitates the process basics understanding for optimizing the final process performance. However the complex nature of the EDM process interaction However, the complex nature of the EDM process interaction between the electrode (tool) and the workpiece material

does not facilitate this task. To solve this question many authors have applied statistic methods such as analysis of variance (ANOVA) models and S/N ratios in order to analyze and optimize the process performance measures (process outputs) in comparison of the process parameters (process inputs). Taguchi method is very effective to deal with response influenced by multivariables, which is clearly the case of EDM process The signal-to-noise ratio is a quality ratio that permits to evaluate the effect of changing a particular design parameter on the performance of the process[4][5][6].

M. Kiyak et al, Y Guu et al & M. Mahardika et al studied that EDM-workpiece material interaction is influenced by many process parameters and considered highly non-linear. There are a number of operational parameters which must be set when manufacturing process is done. These operation parameters are variable and can be adjusted in areas to optimize the desired quality of the machined features. However, there have been many studies aimed at systematically investigating the influence of process variables during EDM machining.[7][8][9]. Results given in this paper helps to select appropriate EDM parameters when user designs process planning based on product requirements such as geometrical features and surface roughness.

2. EXPERIMENTAL SETUP.

2.1 The setup

The experiments have been conducted on the Joemars make EDM machine. The machine is equiped with fuzzy controller to get a hold of utmost accuracy during the operation. Fig 1 shows the main parts and overall set up of the experimental work.



Fig. 1 JOEMARS EDM Machine

2.2 Workpiece material

To conduct experiments we make use of AISI H13 steel of 6 mm thick size. The reason behind selection of this material is the vast application of this material in Extrusion tools, Forging Dies, Plastic moulds, Die casting Dies. Mandrels, Ejector pin.etc.. The Chemical compositions of AISI H13 steel as per testing by Divine Laboratory Services, Ahmedabad given in table 1.

Table 1 Chemical composition of AISI H13 steel

Composition In %	С	Si	Mn	Cr	Мо	V
	0.40	0.97	0.45	5.30	1.35	0.80

2.3 Electrode material

Among the various metallic and non metallic electrode, copper electrode with 15 mm diameter was selected as tool. Its material characteristics are listed below.

- Melting point at 1083°C
- Density = 8.9 g/cm3
- Electrical resistivity of 0.0167 ohm mm2/m
- Coefficient of expansion of 4.318 X 10-4 mm mm/°K

Copper is machinable but wheel loading in grinding seriously affect surface finish and accuracy. Copper is most often used when high surface finish in work material is required. The tool can be policed to about 0.25 micron Ra to provide best surface integrity in the work Material.

2.4 Electrode Geometry

There are four different electrode geometry is taken into consideration. They are Round(C) – \emptyset 15, Square(S) – 15 x 15, Rectangle(R) – 15 x 19, Triangle (T) – 15 x 15 x 15. The dimensiones are in mm.

2.5 Surface Roughness

Surface topography or surface roughness, also known as surface texture are terms used to express the general quality of a machined surface, which is concerned with the geometric irregularities and the quality of a surface [9]. Surface Roughness measures as the arithmetic average, Ra (μ m).



Fig. 2 Mitutoyo SJ210P surface roughness tester.

Fig. 3 precise weighing machine

The Ra value, also known as centre line average (CLA) and arithmetic average (AA) is obtained by averaging the height of the surface above and below the centre line. The Ra will be measured using a surface roughness tester from Mitutoyo, Model: SJ 210P. The Ra values of the WEDMed surface were obtained by averaging the surface roughness values of 5 mm measurement length.

2.6 Material Removal Rate

It is well-known and elucidated by many EDM researchers by Roethel that Material Removal Mechanism (MRM) is the process of transformation of material elements between the work-piece and electrode. The transformation are transported in solid, liquid or gaseous state, and then alloyed with the contacting surface by undergoing a solid, liquid or gaseous phase reaction.

The material MRR is expressed as the ratio of the difference of weight of the workpiece before and after machining to the machining time and density of the material.

$$MRR = \frac{\Psi_{tb} - W_{ta}}{D \times t}$$

Where, W_{tb} = Weight before machining in gm, W_{ta} = Weight after machining in gm, D = Density of work piece material in gm/m³, t=time consumed for machining in minute.

The weight of the work piece and tool is measured on precise weighing machine having least count of 0.001 gm.

3. DESIGN OF EXPERIMENTS.

To determine influential parameters for EDM groove machining, 24 experiments have been carried out based on Taguchi Orthogonal Array $OA_{16}(4^5)$ has been chosen in order to have representative data[11]

Gap Voltage, Current Intensity, Pulse on time, pulse off time are influential parameter to the common performance measures like MRR and Surface roughness [10]. In addition, tool geometry is also considered to identify its influence on these process performance measures and especially on final accuracies. Table 2 presents the five different EDM process parameters chosen and their levels. The rest of EDM parameters, presented in Table 3, must be kept constant during the experimentation to ensure a right comparison between the 24 tests.

The Taguchi method aims to find an optimal combination of parameters that have the smallest variance in performance. The signal-to-noise (S/N) ratio measures how the response varies relative to the nominal or target value under different noise conditions.

Table 2 EDM process parameters and levels								
Parameter	Level							
	L1	L2	L3	L4				
Gap Voltage(V)	16	12	8	4				
Current Intensity (A)	50	43	36	28				
Pulse on time(µs)	22	42	52	62				
Pulse off time(µs)	22	32	42	52				
Tool Geometry.	ROUND	SQUARE	RECT.	TRIANG LE				

Table 3 Constant EDM parameters							
Parameter	Level						
Polarity	+						
Servo Sensitivity	7						
Flushing Height	10						
Working Time	10						
Low Wear Factor	0						

The analysis of variance (ANOVA) is the statistical treatment most commonly applied to the result of the experiments to determine the percentage contribution of each factors. Study of ANOVA table for a given analysis helps to determine which of the factors need control and which do not. Once the optimum condition is determined, it is usually good practice to run a confirmation experiments. Analysis provides the variance of controllable and noise factors. By understanding the source and magnitude of variance, robust operating condition can be predicted.

V	Α	Pon	\mathbf{P}_{off}	Tool	SR	S/N (Ra)	MRR	S/N
								(MRR)
16	50	22	22	С	8.561	-18.6505	54.23	34.68479
16	43	42	32	S	6.047	-15.6308	36.54	31.25537
16	36	52	42	R	3.014	-9.58286	39.63	31.96048
16	28	62	52	Т	2.335	-7.36574	35.35	30.96779
12	50	42	42	Т	8.304	-18.3857	50.73	34.1053
12	43	22	52	R	3.105	-9.84123	44.48	32.9633
12	36	62	22	S	2.325	-7.32846	27.36	28.74232
12	28	52	32	С	9.14	-19.2189	26.46	28.4518
8	50	52	52	S	7.921	-17.9756	43.74	32.81758
8	43	62	42	С	5.513	-14.8278	45.64	33.18691
8	36	22	32	Т	2.63	-8.39911	40.29	32.10395
8	28	42	22	R	2.223	-6.93879	38.38	31.6821
4	50	62	32	R	8.507	-18.5955	38.42	31.69115
4	43	52	22	Т	6.503	-16.2623	35.65	31.04119
4	36	42	52	С	5.648	-15.0379	48.95	33.79505
4	28	22	42	S	3.688	-11.3358	25.61	28.16819
8	50	42	22	R	8.726	-18.8163	57.86	35.24757
12	43	62	42	С	6.981	-16.8784	48.62	33.7363
4	36	52	32	S	6.595	-16.3843	40.21	32.08668
16	50	62	22	Т	10.531	-20.4494	53.93	34.63661
8	36	52	32	С	6.261	-15.9329	31.05	29.84123
12	28	62	52	R	3.75	-11.4806	35.63	31.03632
4	28	52	52	S	2.84	-9.06637	35.49	31.00212
16	28	22	22	R	3.208	-10.1247	15.48	23.79542

Table 4 Experimental results and respective S/N ratio of the 24 Experiment for Surface roughness and MRR.

C-Round, S-Square, R-Rectangle, T-Triangle

 Table 5 ANOVA for surface roughness.

Source	DF	Seq SS	Adj SS	Adj MS	F	Р
A	3	2.241	19.48	6.493	0.89	0.487
В	3	248.555	247.12	82.373	11.28	0.003
С	3	38.594	27.49	9.165	1.26	0.353
D	3	42.810	32.50	10.833	1.48	0.291
G	3	65.718	65.72	21.906	3.00	0.095
Residual Error	8	58.414	58.41	7.302		
Total	23	456.332				

	Α	В	С	D	G
1	-14.45	-10.79	-11.67	-14.08	-16.76
2	-13.82	-12.11	-14.96	-15.69	-12.95
3	-13.86	-14.69	-14.92	-14.20	-12.20
4	-13.63	-18.81	-13.85	-11.79	-14.17
Delta	0.81	8.02	3.29	3.90	4.56
Rank	5	1	4	3	2

Table 6 Response Table for Signal to Noise Ratios (Smaller is better)

Table 7 ANOVA for MRR

Source	DF	Seq SS	Adj SS	Adj MS	F	Р
А	3	6.114	1.867	0.6225	0.11	0.951
В	3	67.888	56.761	18.9204	3.39	0.074
С	3	9.929	8.994	2.9981	0.54	0.670
D	3	14.973	16.003	5.3345	0.95	0.459
G	3	5.944	5.944	1.9812	0.35	0.787
Residual Error	8	44.698	44.698	5.5872		
Total	23	149.546				

Table 8 Response Table for Signal to Noise Ratios (Larger is better)

	Α	В	С	D	G
1	31.30	29.30	30.34	31.40	32.28
2	32.48	31.42	33.22	30.91	30.68
3	31.51	32.44	31.03	32.23	31.20
4	31.22	33.86	32.00	32.10	32.57
Delta	1.26	4.56	2.87	1.33	1.89
Rank	5	1	2	4	3

4. RESULT AND DISCUSSION.

All 24 experiments are carried out by the process parameters shown in Table 2 and Table 3.Table 4 shows the final results of five input variable like, Gap voltage(V), Current Intensity (A), Pulse on time (μ s), Pulse off time (μ s) and Tool Geometry. S/N ratio is give for Surface roughness and MRR.

Table 5 and Table 7 present the final results of ANOVA. From this Table we can see the pvalue for B is 0.003 so this is most significant parameter that affects surface roughness. It is same for MRR that p-value for B is less than others so it is the most significant factor and it is Current intensity.

Table 6 and Table 8 present the response table for S/N ratio for Surface roughness and MRR. From this rank is provided that which parameter affects the most to the least.

For Surface roughness it is 1. Current intensity 2. Tool Geometry .3. Pulse off time 4. Pulse on time 5. Gap voltage.

For MRR it is 1. Current Intensity 2. Pulse on time 3.Tool Geometry. 4. Pulse off time 5. Gap Voltage. From these results we can say that Tool Geometry is the significant factor for the Material Removal Rate and Surface Roughness





Figure 4 Comparison of MRR and SR with current intensity at different tool geometry.

Figure 4 shows that as current intensity increases the MRR increases and so the surface Quality is decreases. Both the graph shows a same result that is the basic rule. But for current

intensity 36 the results are different and the MRR is good and Surface Quality also good tor triangle and Rectangle Geometry.





Figure 5 Comparison of MRR and SR with pulse off time at different pulse on time.

Fig. 5 shows that as the pulse on time and pulse off time difference increases the MRR and SR both give negative results that MRR decreases and SR increases. But as they come nearer to each other both the output parameter showing good results.

5. CONCLUSION

Influence of process parameters (Gap voltage, Current intensity, Pulse on time, pulse off time, Tool Geometry) on MRR and Surface roughness has been analyzed for copper electrode and AISI H13 workpiece material on sinking EDM process using ANOVA.

Tool geometry is not the most significant factor that affects the performance measures the most but it is a significant factor that affects the performance measures.

As per the S/N ratio and ANOVA the percentage contribution of the tool Geometry is varies from 10% to 20%.By this we can say that by changing the geometry we can get better MRR & SR up to certain extent From Fig. 4 The Rectangle Geometry at 43 A current give good results for both the performance measures.

Now, Pulse on time and Pulse off time range is also affects the MRR and SR.At $P_{ON}=22$ & $P_{OFF}=22$ we get good results but at $P_{ON}=22$ & $P_{OFF}=62$ we cannot achieve that much good results.

6. REFERENCES:

1. Ozgedik, A. (2006). An Experimental investigation on tool wears in electric discharge machining. International Journal of Advanced Manufacturing Technology, 27, 488-496.

3. Yan, B. H., Huang, F. Y., Chow, H.M., & Tsai, J. Y. (1999). Micro-hole machining of carbide by electrical discharge machining. Journal of Materials Processing Technology, 87(1-3), 139-145.

4. Lin, Y., Cheng, C., Su B., & Hwang, L. (2006). Machining characteristics and optimization of machining parameters of SKH 57 high-speed steel using electrical-discharge machining based on Taguchi method. Materials Manufacturing Processes, 21(8), 922-929.

5. Sundaram, M. M., Pavalarajan, G. B., & Rajurkar, K. P. (2008). A study on process parameters of ultrasonic assisted micro EDM based on Taguchi method. Journal of materials Engineering perform, 17(2), 210-215.

6. Pradhan, B. B. Masanta, M., Sarkar, B. R., Bhattacharyya, B. (2008). Investigation of electrodischarge micro-machining of titanium super alloy. International Journal advanced Manufacturing technologies 1-13.

7. Kiyak, M., & Cakir, O. (2007). Examination of machining parameters on surface roughness in EDM of tool steel. Journal of Materials Processing Technology, 191(1-3), 141-144.

8. Guu Y. H., & Hou, M. T. (2007). Effect of machining parameters on surface textures in EDM of Fe-Mn-Al alloy. Materials Science Engineering, 466(1-2), 61-67.

9. Mahardika, M., Tsujimoto, T., & Mitsui, K. (2008). A new approach on the determination of ease of machining by EDM processes. International Journal of Machine Tools and Manufacture, 48, 746-760.

10. Salman, O., & Kayacan, M. C. (2008). Evolutionary programming method for the modelling the EDM parameters for roughness. Journal of Materials Processing Technology, 200 (1-3), 347-355.

11. Logothetis, N., & Wynn, H.P. (1989) Quality through design: Experimental design, off-line quality control and Taguchi's contributions. Oxford: Clarendon Press.