

Design and Simulation of High Voltage Gain Buck-Boost Converter for Electric Vehicle using MATLAB

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Abstract: This research describes a revolutionary voltage-lift switched inductor (VLSI) cell-based high step-up DC-DC multilevel buck-boost converter. Cascade of traditional DC-DC converters is not a workable solution to reach high conversion ratio. In this study, a VLSI cell is used to improve the multilevel buck-boost converter's boost capabilities. The suggested DC-DC multilevel topology's key benefit is that it achieves large conversion ratios without the use of coupled inductors, transformers, or high duty cycles. The 200W-rated buck-boost multilevel converter that is being suggested has three stages and a 220V output voltage. The duty cycle is 70%, the switching frequency is 50 kHz, and the input supply voltage is 12 V.

Keywords: Voltage multiplier, voltage-lift switched inductor (VLSI) cell, multilevel buck-boost converter.

I. INTRODUCTION:

The use of a normal DC-DC converter in conjunction with a voltage multiplier cell[10], a voltage raise switching inductor cell, and a five level buck-boost converter allows for large voltage gain. The voltage multiplier cell, also known as a Cockcroft Walton multiplier, is used to generate high output voltage from low level AC or pulsating DC input voltage. Television, particle accelerators, and many other electronic devices still use voltage multiplier cells to obtain high output voltage. X-ray machines, televisions, and photocopiers are a few devices that use voltage multiplier cells[13]. Step up transformers are typically used to get high output voltage, however they are expensive, take up a lot of space, and produce current and voltage with a significant degree of ripple. The voltage multiplier cell resembles a ladder network and is made up of diodes and capacitors.

II. PROPOSED CONVERTER TOPOLOGY

Figure 1 shows the power circuit for a VLSI[14] cell and voltage multiplier-based five-level DC to DC buck boost converter. A single switch, 13 diodes, two inductors, and 10 capacitors are used in the converter design [2]. The five level buck boost converter's key benefit is that high voltage gain is achieved without the use of a transformer, coupled inductor, or an excessive duty cycle.

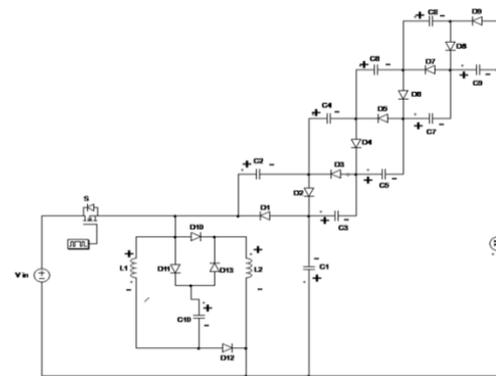


Fig. 1 Five level buck boost Converter.

When switch S is in the ON position, the supply voltage V_{in} will charge both inductors L1 and L2 in parallel through the corresponding diodes D10 and D12[5][8]. Through diodes D11 and D12, supply voltage V_{in} also charges capacitor C10 during this time. When diode D2 is forward biased, the voltage across capacitor C1 charges capacitor C2 across the diode. Finally, voltage across capacitors C1 and C3 charges capacitors C4 through the diode D4. Additionally, voltage across capacitors C1,C3 and C5 charges capacitors C6 through the diode D6, and voltage across[15] capacitors C1,C3,C5, and C7 charges capacitor C8 through the diode D8, resulting in voltage V_0 across capacitors C1,C3,C5,C7 and C9. Figure 2 describes how the switch S operates in mode 1, or when it is turned on.

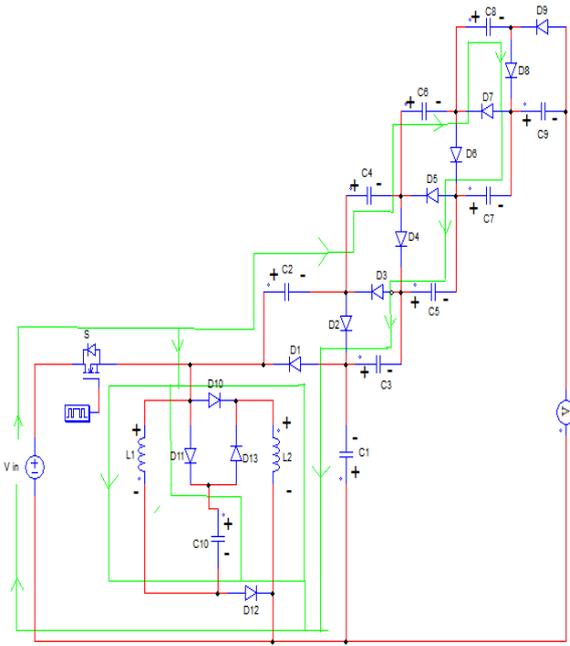


Fig. 2 Mode-1 operation when switch s is ON

There will be no connection between the input power supply and the load while switch S is in the OFF position[3][4]. The inductors L1, L2, and capacitor C10 will be connected in series under this circumstance. This series configuration of capacitor C10, inductors D1, and D13 charges the capacitor C1. A series of inductors L1, L2, capacitors C2, C10, and diodes D3 and D13 charges capacitors C1 and C3 when D3 is forward biased. The series configuration of inductors L1, L2 and capacitors C10, C2, C4, C6 charges the capacitors C1, C3, C5 and C7 through diodes D7 and D13. The series configuration of inductors L1, L2 and capacitors C10, C2, C4, C6 charges the capacitors C1, C3, C5 and C7 through diodes D5 and D13. Finally, the capacitors C1, C3, C5, C7, and C9 are charged through diodes D9 and D13 by the series combination of inductors L1, L2, and capacitors C10, C2, C4, C6, and C8. When switch S is OFF, or in mode 2[6], as shown in Figure 3, the system[11][12] operates.

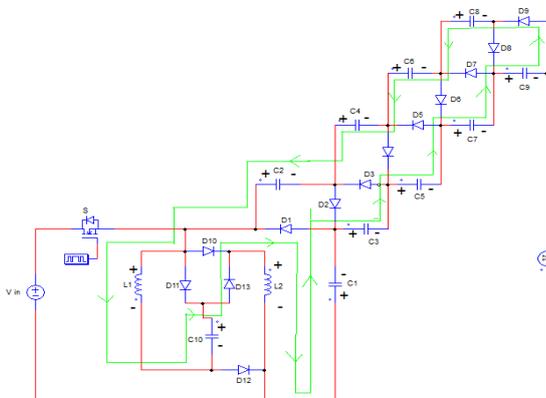


Fig. 3 When switch S is OFF (mode2)

When switch S[1] is in ON condition
 $V_{L1} = V_{in}$ (1)

$$V_{L2} = V_{in} \quad (2)$$

$$V_{L1} = V_{L2} = V_L = V_{in} \quad (3)$$

$$V_{C10} = V_{in} \quad (4)$$

$$V_{C2} = V_{in} + V_{C1} \quad (5)$$

$$V_{C2} + V_{C4} = V_{in} + V_{C1} + V_{C3} \quad (6)$$

$$V_{C2} + V_{C4} + V_{C6} + V_{C8} = V_{in} + V_{C1} + V_{C3} + V_{C5} + V_{C7} \quad (7)$$

$$V_0 = V_{C1} + V_{C3} + V_{C5} + V_{C7} + V_{C9} \quad (8)$$

When switch S is in OFF condition

$$-V_{L1} + V_{C10} - V_{L2} - V_{C1} = 0 \quad (9)$$

$$V_{C3} = V_{C2} \quad (10)$$

$$V_{C3} + V_{C5} = V_{C2} + V_{C4} \quad (11)$$

$$-V_{L1} + V_{C10} - V_{L2} - V_{C1} - V_{C3} - V_{C5} + V_{C4} + V_{C2} \quad (12)$$

$$V_{C3} + V_{C5} + V_{C7} = V_{C2} + V_{C4} + V_{C6} \quad (13)$$

$$-V_{L1} + V_{C10} - V_{L2} - V_{C1} - V_{C3} - V_{C5} - V_{C7} + V_{C6} + V_{C4} + V_{C2} \quad (14)$$

$$V_{C3} + V_{C5} - V_{C7} - V_{C9} = V_{C2} + V_{C4} + V_{C6} + V_{C8} \quad (15)$$

$$-V_{L1} + V_{C10} - V_{L2} - V_{C1} - V_{C3} - V_{C5} - V_{C7} - V_{C9} - V_{C8} + V_{C6} + V_{C4} + V_{C2} \quad (16)$$

Substitute equation (3) in (9)

$$V_L = \frac{V_{C10} - V_{C1}}{2} \quad (17)$$

By inductor volt second balance

$$V_{in}D + \frac{V_{C10} - V_{C1}}{2}(1-D) = 0 \quad (18)$$

$$V_{C1} = \frac{2V_{in}D}{1-D} + V_{C10} \quad (19)$$

$$\frac{V_{C1}}{V_{in}} = \frac{2D}{(1-D)} = \frac{V_{C10}}{V_{in}} \quad (20)$$

Substitute equation (4) in (20)

$$\frac{V_{C1}}{V_{in}} = \frac{2D}{(1-D)} + 1 = \frac{1+D}{1-D} \quad (21)$$

Substitute equation (5) in (21)

$$\frac{V_{C2}}{V_{in}} = \frac{2}{(1-D)} \quad (22)$$

Substitute equation (10) in (22)

$$\frac{V_{C3}}{V_{in}} = \frac{2}{(1-D)} \quad (23)$$

Similarly from (6) and (11)

$$\frac{V_{C4}}{V_{dc}} = \frac{V_{C5}}{V_{dc}} = \frac{2}{(1-D)} \quad (24)$$

$$V_{C2} = V_{C3} = V_{C4} = V_{C5} = V_{C7} = V_{C9} = \frac{2V_{in}}{1-D} \quad (25)$$

$$\frac{V_{out}}{V_{in}} = \frac{V_{C1}}{V_{in}} + \frac{V_{C3}}{V_{in}} + \frac{V_{C5}}{V_{in}} + \frac{V_{C7}}{V_{in}} + \frac{V_{C9}}{V_{in}} \quad (26)$$

Thus voltage gain ratio for five level buck boost converter is

$$G_5 = \frac{9+D}{(1-D)} \quad (27)$$

IV. DESIGN DETAILS:

The five level buck boost converter has been designed for 200W load and 400V output voltage. The duty cycle needed to get 400V output voltage from 12V input will be 70.8% with a switching frequency of 5KHZ [7].

$$R = \frac{(V_o)^2}{P} = \frac{400^2}{200} = 800\Omega$$

the critical inductance LC value is calculated from below expression

$$L_{C1} = L_{C2} = \frac{(1-D)R}{2f}$$

Where, f = Swiching frequency in Hertz

R = Resistive load in ohm

The critical inductance value will depends on duty ratio, switching frequency and resistive load.

$$L_{C1} = L_{C2} = \frac{(1-0.708)(800)}{2*5000} = 25mH$$

The critical capacitance value can be obtained from the below expression[4]

$$C_{critical} \gg \frac{N^2}{\pi^2 f_s^2 L}$$

$$C_{critical} = \frac{5^2}{\pi*(5K^2)(25m)} = 310*10^{-6} F$$

The five level buck boost converter specification details for 200W load is given in table 1

Table 1 Five level buck boost converter specification

Power	200W
Input Voltage	12 volts
Input Current	16 ampere
Duty cycle	70.8
Output Voltage	400 volts
Output Current	0.5 ampere
Inductors	25mH
Capacitors	330μF

DC motor specification details given in table 2 is used as a load for five level buck boost converter

Table 2 DC motor specification

Power rating	150W
Armature voltage	400V
Field voltage	400V
No load current	0.198A
Full load current	0.5A
No load speed	1375rpm
Full load speed	1284rpm
Full load torque	0.8N-M

V. SIMULATION RESULTS:

Open loop SIMULINK model of five level buck boost converter with resistive load

DC to DC five level buck boost converter with 800Ω resistive load is designed to get output voltage of 400V from input voltage of 12V. The SIMULINK model is shown in Figure 4. It consists of one ideal switch (with internal diode resistance Ron= 0.001Ω & Snubber resistance Rs=1e⁵Ω), two 25mH inductor with 0.05Ω series resistor, ten number of 330μF capacitors and thirteen number of diodes (with internal diode resistance Ron=0.001Ω & Snubber resistance Rs=1e⁵Ω). Duty cycle of 70.8% is required to get 400V output voltage from 12V input voltage.

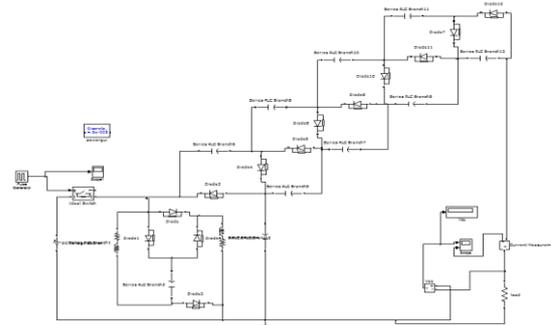


Fig. 4 SIMULINK model of open loop five level buck boost converter with resistive load

The five level buck boost converter is fed with input voltage of 12V with 800Ω resistive load. The response of converter in the given case is shown in the Figure 5 and 6

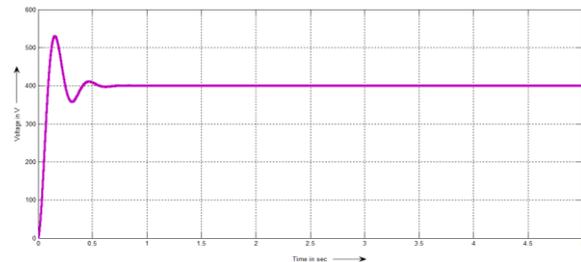


Fig. 5 Output voltage

Figure.5 shows voltage waveform drawn regarding with time. From the result, it is observed that the overshoot (%)

value of output voltage will be 32.87% and settle to 400V at a settling time of 0.7S.

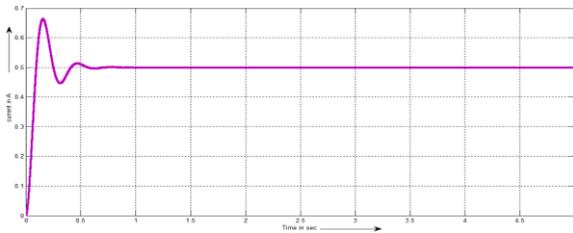


Fig. 6 Output current

Figure.6 shows current waveform drawn regarding with time. From the result, it is observed that the overshoot (%) value of output current will be 32.94% and settle to 0.5A at a settling time of 0.7S.

SIMULINK model of closed loop five level buck boost converter with resistive load

Five level buck boost converter with resistive load designed to get output voltage of 400V. The SIMULINK model is shown in Figure 7. It consists of one ideal switch (with internal diode resistance $R_{on}=0.001\Omega$, Snubber resistance $R_s=1e^5\Omega$), two 25mH inductor with 0.05Ω series resistor, ten number of 330 μ F capacitors and thirteen number of diodes (with internal diode resistance $R_{on}=0.001\Omega$ & Snubber resistance $R_s=1e^5\Omega$). Here PI controller is used to set constant output voltage under variable loads.

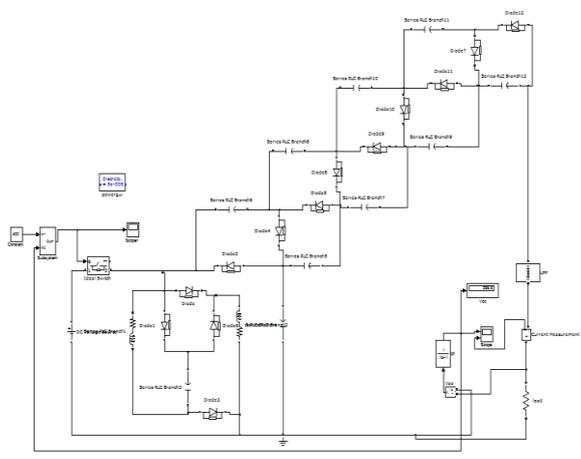


Fig. 7 Closed loop SIMULINK model of DC to DC five level buck boost converter with resistive load

Here PI controller is used to get constant speed under variable loads. Here the output speed is sensed and compared with the reference speed which gives error signal. Then the error signal is than given to PI controller by setting $K_p=5$ and $K_i=5$ value. The output of PI controller is multiplied with pulse generator which is of 70.8% duty cycle and switching frequency of 5KHZ which gives the gate pulse for ideal switch.

The DC-DC five level buck-boost converter is fed with input voltage of 12V with 800 Ω resistive load. Here PI

controller is used to maintain constant output voltage of 400V under variable loads. The response of converter in the given case is shown in the Figure 8 and 9.

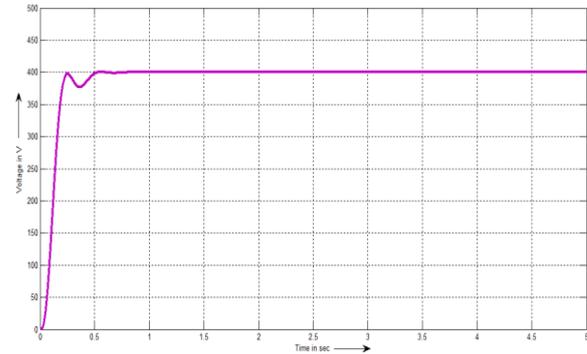


Fig. 8 Output voltage

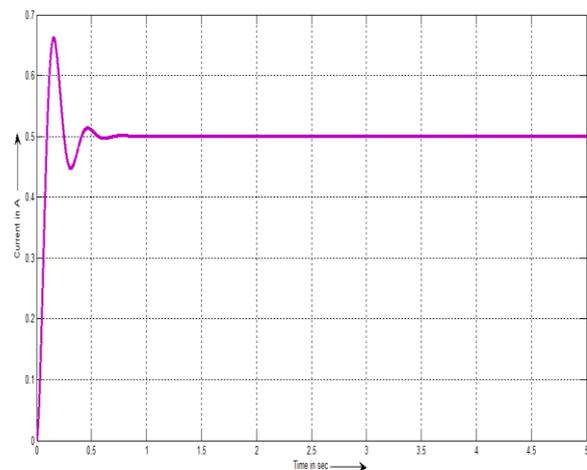


Fig. 9 Output current

Table 3 Five level buck-boost converter with resistive load test conditions

Output voltage in V	Output current in A	Resistive load in Ω
400	0.5	800
403.4	0.448	900
405.3	0.405	1000
406.7	0.37	1100
408	0.34	1200
418	0.052	8K
420	5.25	800K

Results for open loop DC to DC five level boost converter with DC motor as a load

The DC to DC five level buck boost converter is fed with input voltage of 12V with 150W DC motor at no load. The response of converter with DC motor in the given case is shown in the Fig 10(a, b, c, d, and e)

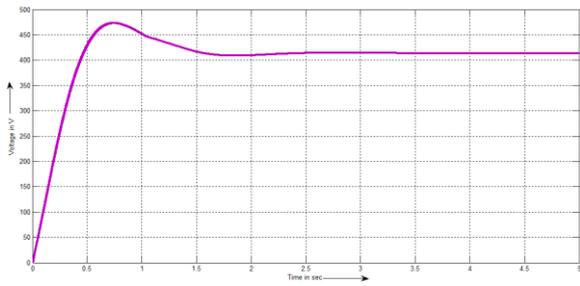


Fig 10 (a) Output voltage

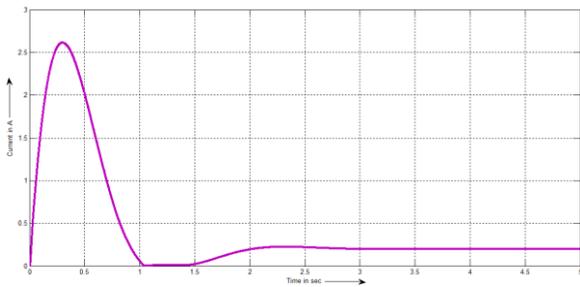


Fig 10 (b) Output current

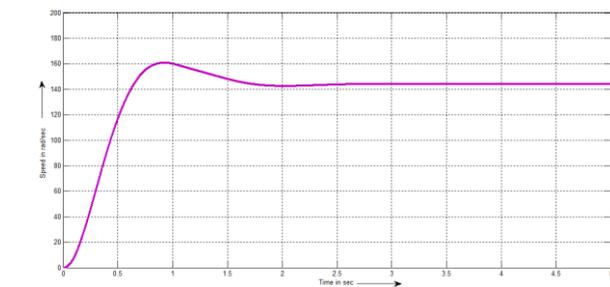


Fig 10 (c) Output speed

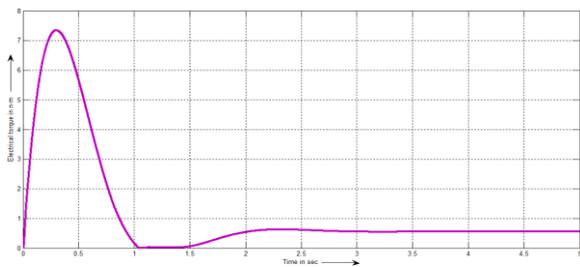


Fig 10 (d) Electrical torque

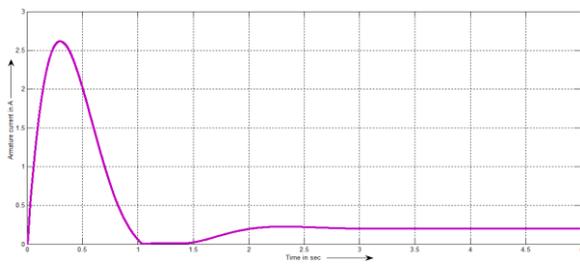


Fig 10 (e) armature current

Table 10.1 Five level buck boost converter with DC motor load test conditions

10.1.1 Results for closed loop DC to DC five level buck boost converter with DC motor as a load for constant output voltage

The DC-DC five level buck-boost converter is fed with input voltage of 12V with 150W DC motor at no load. Here PI controller is used to maintain constant output voltage of 400V under variable loads. The response of converter in the given case is shown in the Fig 10.1.1 (a, b, c, d and e)

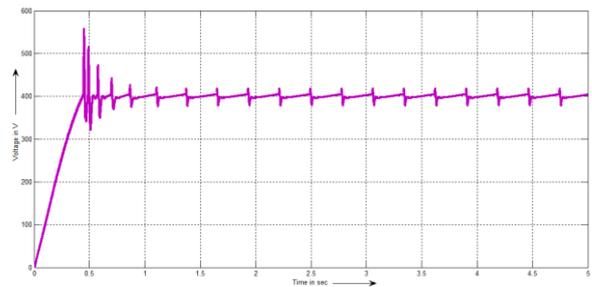


Fig 10.1.1 (b) Output current

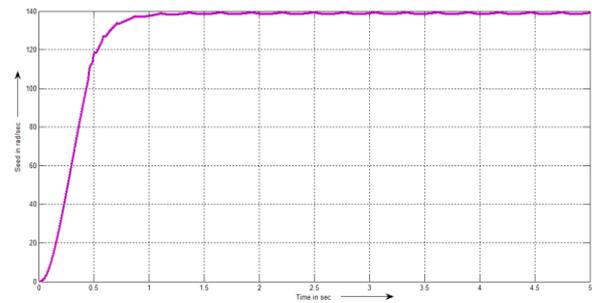


Fig 10.1.1 (c) Output speed

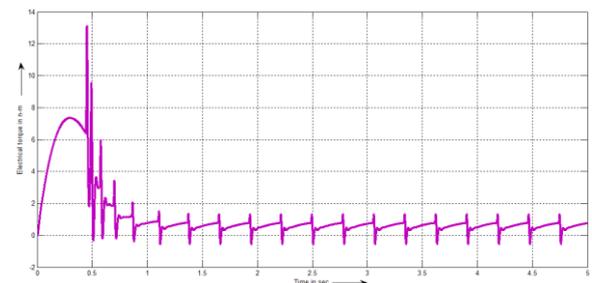


Fig 10.1.1 (d) Electrical torque

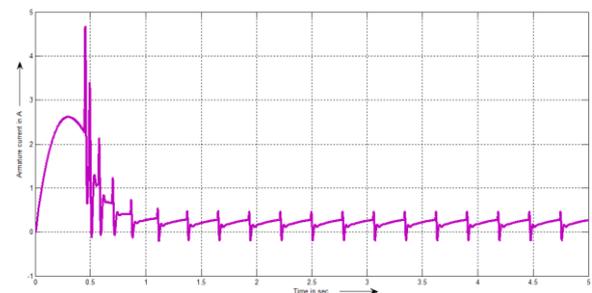


Fig 10.1.1 (e) armature current

6.4.5 Results for closed loop DC to DC five level buck boost converter with DC motor as a load for constant speed output

The DC-DC five level buck-boost converter is fed with input voltage of 12V with 150W DC motor at no load. Here PI controller is used to maintain constant speed $139w_m$ under variable loads. The response of converter in the given case is shown in the Fig 11(a, b, c, d & e)

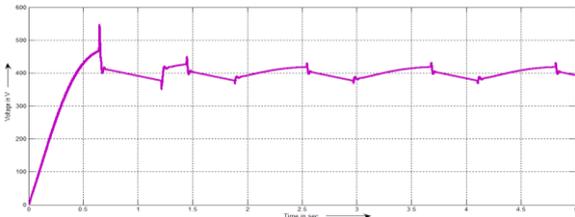


Fig 11(a) Output voltage

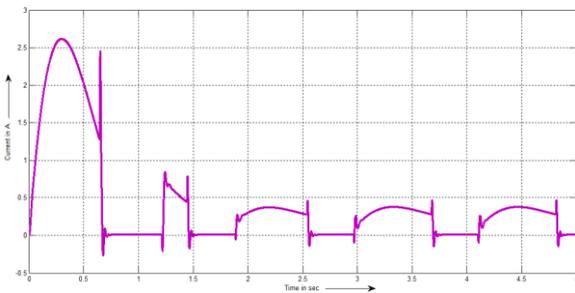


Fig 11 (b) Output current

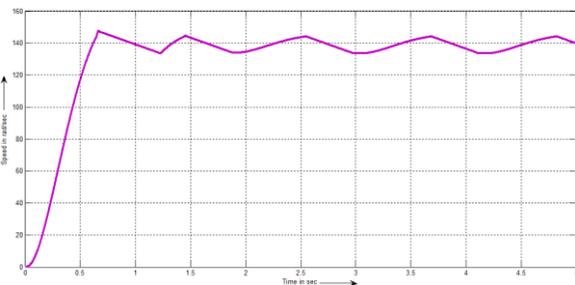


Fig 11 (c) Output speed

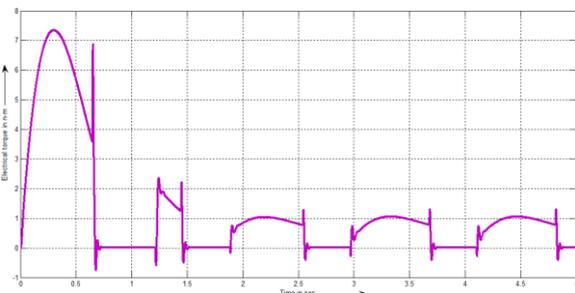


Fig 11 (d) Electrical torque

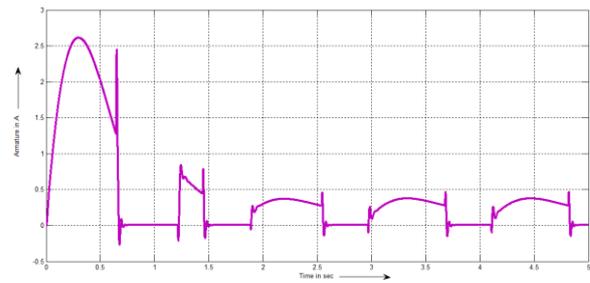


Fig 11 (e) armature current

VI. CONCLUSION

The voltage-lift switched-inductor cell is used to improve the five level buck boost converter's boost capacity. This converter topology is appropriate for applications requiring unidirectional power transfer and high gain supply voltage escalation. When compared to traditional buck boost converters, this converter offers high gain for a specific number of levels. The duty cycle and number of output levels affect the gain of the five-level buck-boost converter. To maintain a steady output with changing loads, PI controllers are employed. The software programme MATLAB / Simulink was used to simulate the DC-DC five buck-boost converter for resistive load with PI controller to maintain constant output voltage under fluctuating load.

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