

Common Mode Feedback for Fully Differential Amplifier in ami06 micron CMOS process

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Abstract— This paper is about the design of the schematic of a common mode feedback for fully differential amplifier. The circuit is designed using CMOS ami06 technology in Cadence. The circuit is optimized to provide a Figure of Merit of $100.74 \times 10^9 \text{ Hz/A}$ and phase margin more than 60 degrees. The layout of the design is done and the LVS match is obtained.

Index Terms— Common-mode feedback, Extracted file, Fully differential amplifier, CMOS ami06 technology, DC analysis, LVS match, STB simulation

I. INTRODUCTION

A Fully differential amplifier is a DC-coupled high-gain voltage amplifier which has differential inputs and differential outputs. A common-mode feedback circuit senses the common mode voltage and compares it with a reference and feeds it back to the correcting common mode signal as to cancel the output common mode current component and to fix the dc outputs to the desired level.

Common mode feedback network consists of a simple feedback which stabilizes the common mode voltage without affecting the differential mode operation of the circuit. Referring to Fig1, if the common mode voltage at node V_{out1} increases, the current through transistor M10 increases thereby reducing the current through M13 transistor. Since the gate voltages of M13 and M3 transistors are the same, the gate voltage of M3 increases thereby decreasing the voltage at the drain of M3 due to inversion. Thus, the V_{out1} value is decreased to the desired level.

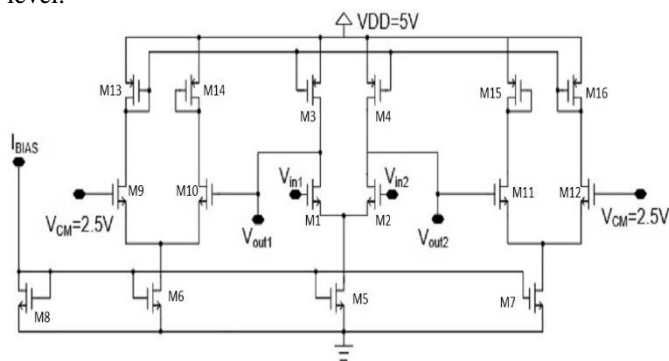


Fig1: Common mode feedback for fully differential amplifier

II. DESIGN AND CIRCUIT ANALYSIS

A. Transistor Sizing

The size of a transistor is determined by its W/L ratio. The ratio of size of transistor M5 to size of transistor M8 should be large to allow more current flow through the differential pair to obtain high gain. The current through M5 is equally divided between transistors M1 and M2. Size of transistors M1 and M2 should be more to achieve high gain. The sizes of other transistors should be chosen to ensure that sufficient current flows through them to operate in active region.

Transistors	Width	Length
M1, M2	4*12 μm	1.95 μm
M3, M4	8*4.05 μm	1.95 μm
M5	8*7.95 μm	1.95 μm
M6, M7	4*7.95 μm	1.95 μm
M8	1*7.95 μm	1.95 μm
M9, M10, M11, M12	4*6 μm	1.95 μm
M13, M14, M15, M16	4*4.05 μm	1.95 μm

Table1: Transistor sizes

B. Bias Current

A bias current is provided at the drain of transistor M8 which is then mirrored to transistors M5, M6, M7 depending on the ratio of their sizes. The value of the bias current chosen is $5\mu\text{A}$. This value is chosen to mirror sufficient current so that all the transistors are in active region and the total DC current consumption is less to optimize the Figure of Merit(FOM).

III. CIRCUIT SIMULATION

Circuit is simulated using Cadence software. The schematic of the common mode feedback for fully differential amplifier circuit is setup with desired transistor sizes and bias current as shown below.

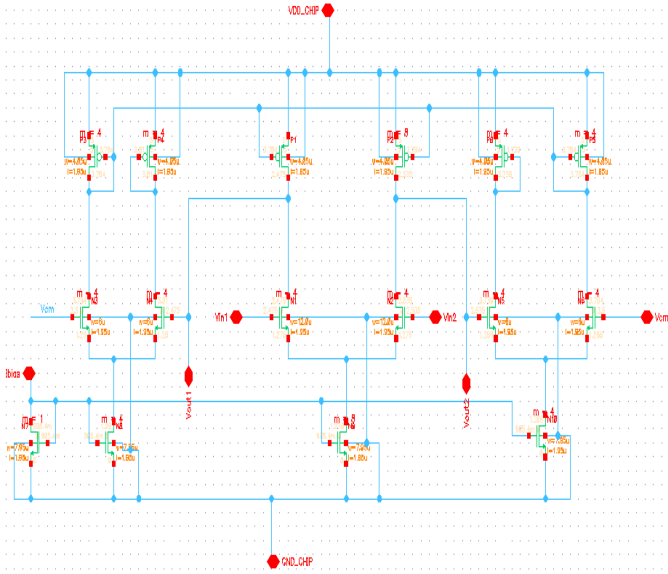


Fig2: Schematic with transistor sizes

DC simulation is performed using spectre simulator. The DC operating points and DC node voltages are annotated.

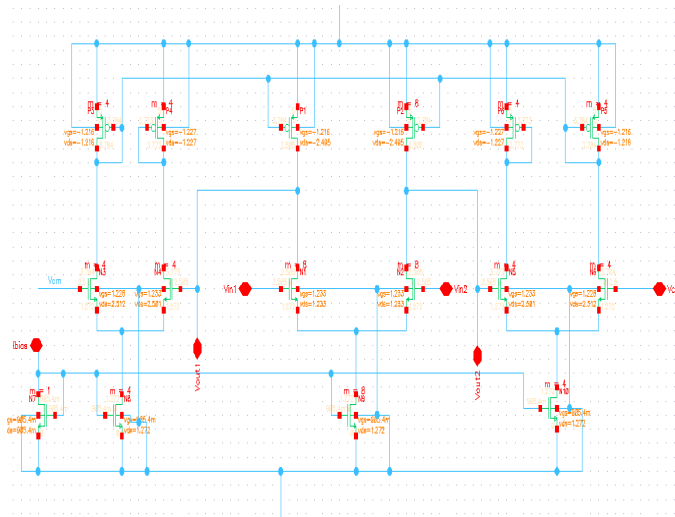


Fig3: Schematic with DC node voltages

Transistors	Current
M1 M2 M3 M4 M6 M7	20.32 μ A
M9 M12 M13 M16	9.747 μ A
M10 M11 M14 M15	10.57 μ A
M5	40.63 μ A
M8	5 μ A

Table2: Currents flowing through transistors

IV. GAIN AND PHASE MARGIN OF DIFFERENTIAL AND COMMON MODE FEEDBACK LOOPS

The figure below is used as a test bench to simulate differential and common mode loop gains.

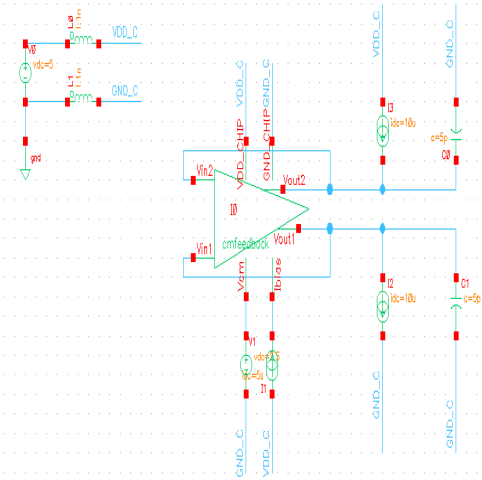


Fig4: Test bench

Transistors	Current(μ A)
M1	10.34 μ A
M2	30.3 μ A
M3	20.34 μ A
M4	20.3 μ A
M5	40.64 μ A
M6	20.31 μ A
M7	20.33 μ A
M8	5 μ A
M9 M12 M16	9.747 μ A
M10 M11 M14 M15	10.57 μ A

Table3: Currents through transistors after introducing test bench

A. Differential mode feedback loop

To obtain the gain and phase plots of differential mode feedback loop, we introduce a CMDM probe in the schematic such that both the common mode and differential mode loops are broken. STB analysis is performed using spectre simulator to obtain the gain and phase plots.

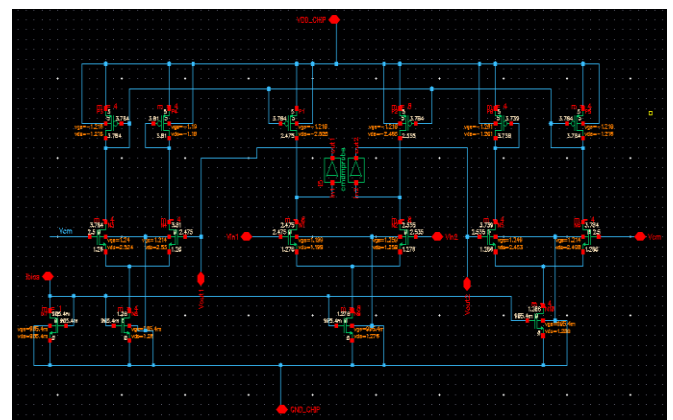


Fig5: Schematic with CMDM probe

To calculate phase margin and gain of differential mode feedback loop, the CDF parameter value in CMDM probe is set to -1.

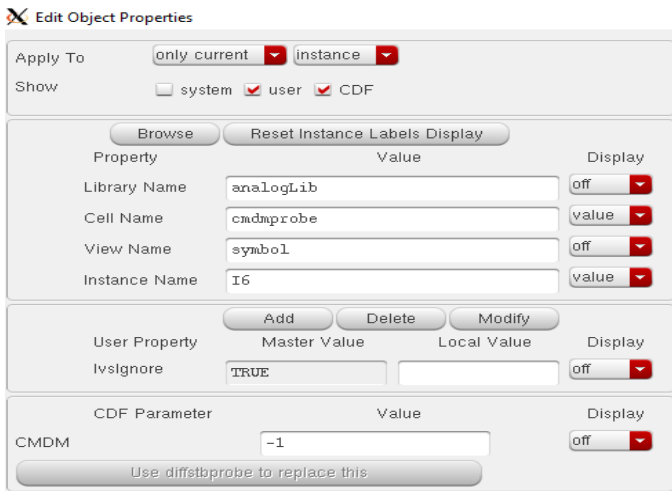


Fig6: CMDM probe Edit Object Properties window

For differential mode, a Gain of 46.946db and a Phase Margin of 88.6425deg is obtained.

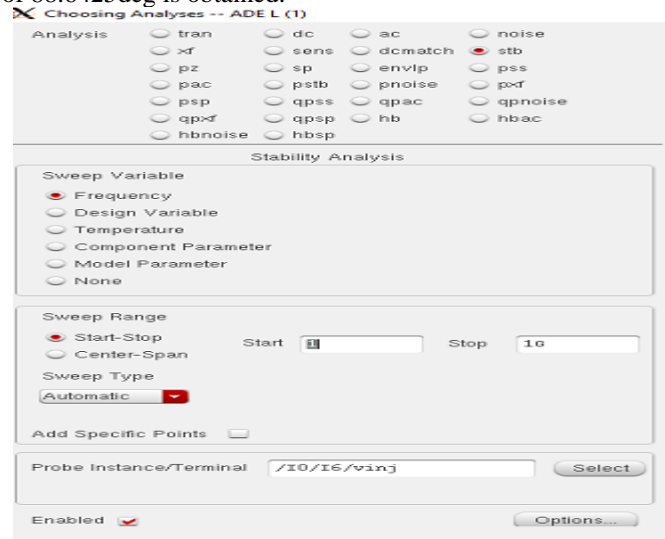


Fig7: STB simulation window

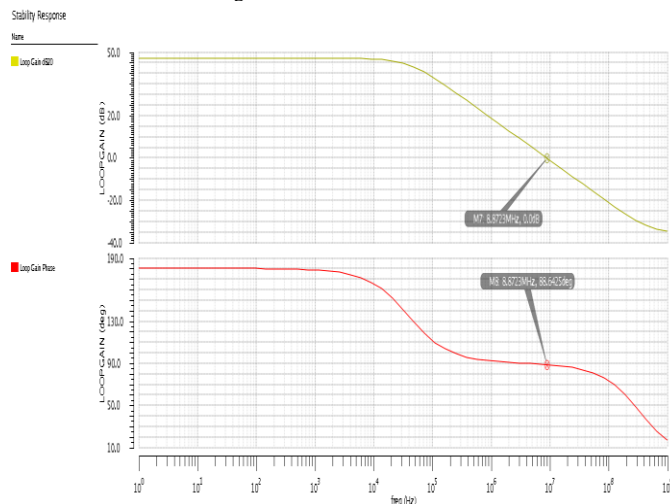


Fig8: Gain and Phase plot of differential mode feedback

B. Common mode feedback loop

To measure the gain and phase margin of common mode feedback loop, the CDF parameter value of CMDM probe is set

to 1. A gain of 49.8712db and a Phase Margin of 83.3384deg is obtained.

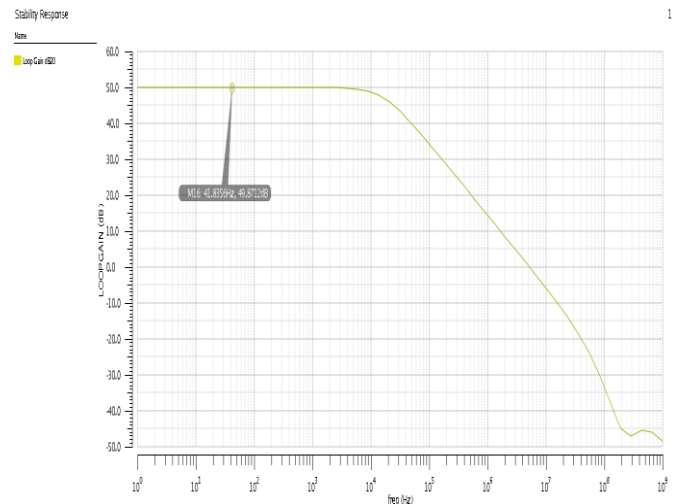


Fig9: Common mode feedback Gain

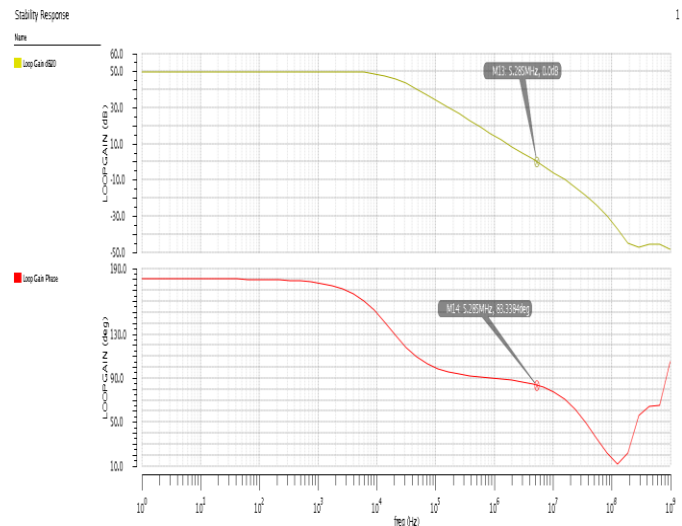


Fig10: Common mode feedback Phase Margin

Loop	Gain	Phase Margin
Differential mode	46.946db	88.6425deg
Common mode	49.8712db	83.3384deg

Table4: Values of gain and phase margin

C. Figure of Merit

Figure of Merit (FOM) is defined as the ratio of Gain Bandwidth product to the total DC current. Figure of merit of differential mode gain is calculated. The total DC current is measured as 86.27μA. The obtained bandwidth is 39.0634KHz. The Gain Bandwidth is 8691MHz. The Figure of Merit is 100.74*10⁹Hz/A.

Parameter	Value Obtained
DC current	86.27μA
Gain	46.946db
Bandwidth	39.0634KHz
Gain Bandwidth	8691MHz
Figure of Merit	100.74*10 ⁹ Hz/A

Table5: FOM parameter values

V. LAYOUT, DRC AND LVS

A. Layout

Layout is designed using common centroid technique with multi fingered gates. The advantages of common centroid layout are immunity from cross-chip gradients, best-matching performance possible and reduced area by sharing the sources. Multi fingered gates are used to reduced series resistance in gate and minimize drain-to-bulk parasitic capacitance.

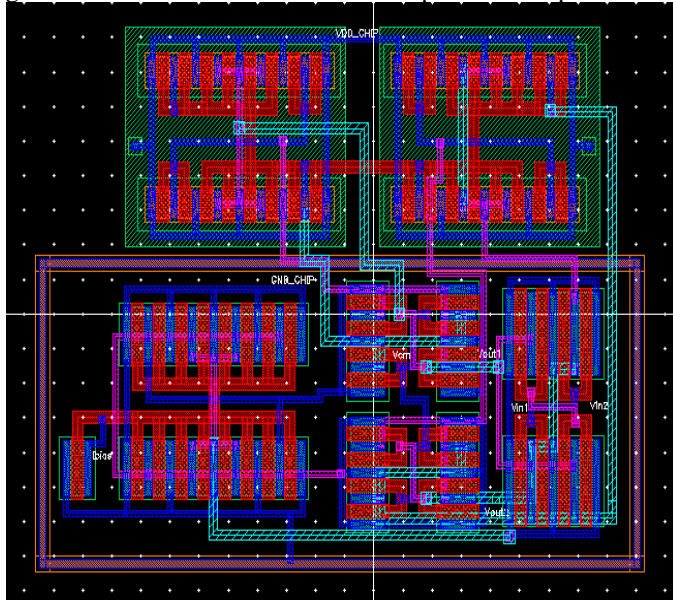


Fig11: Layout

B. DRC

DRC stands for Design Rule Check. It is used to determine whether the layout satisfies the recommended design rules.

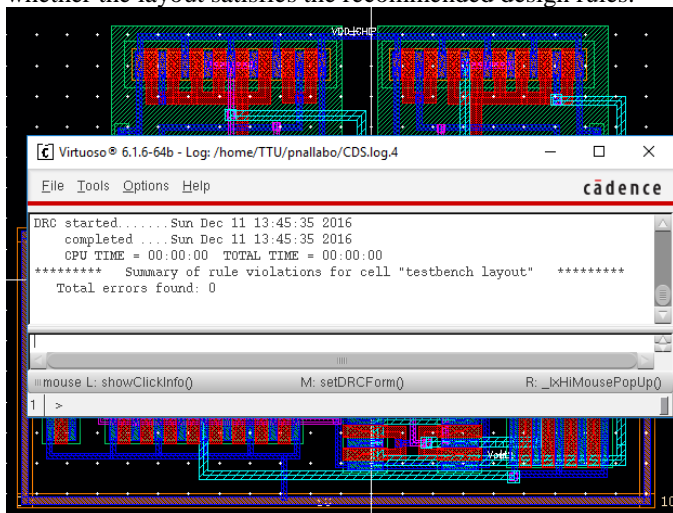


Fig12: CDS.log window showing 0 DRC errors

schematic.

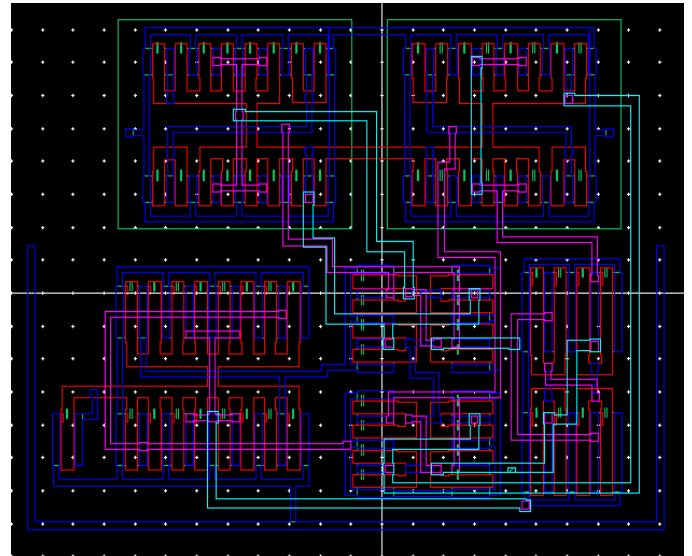


Fig13: Extracted Layout

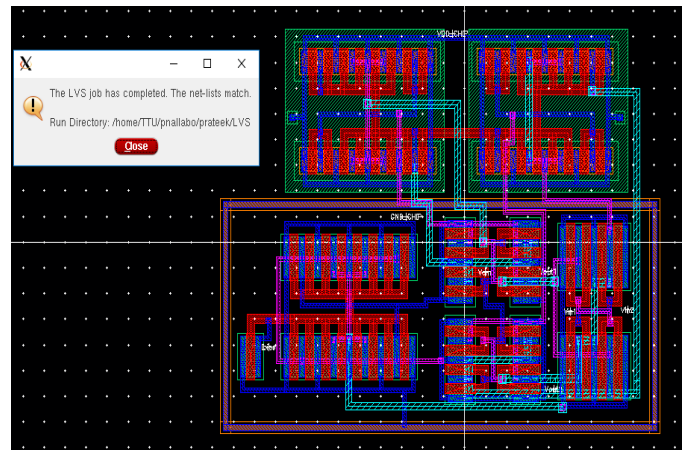


Fig14: Window showing LVS match

```
Net-list summary for /home/TTU/pnallabo/prateek/LVS/layout/netlist
count
14      nets
8       terminals
32      pmos
41      nmos

Net-list summary for /home/TTU/pnallabo/prateek/LVS/schematic/netlist
count
14      nets
8       terminals
6       pmos
10      nmos

Terminal correspondence points
N7      N4      GND_CHIP
N11     N1      Ibias
N8      N3      VDD_CHIP
N6      N8      Vcm
N13     N10     Vin1
N12     N13     Vin2
N10     N12     Vout1
N9      N7      Vout2

Devices in the rules but not in the netlist:
cap nfet pfet nmos4 pmos4

The net-lists match.
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Fig14: LVS file

C. LVS

LVS stands for Layout Versus Schematic. LVS match is performed to check if the layout designed matches with the schematic. The extracted layout file is compared with the

VI. RESULTS

A. Differential mode STB analysis:

Gain= 46.946db
Phase Margin= 88.6425deg
Bandwidth= 39.0634KHz
Gain Bandwidth= 8691MHz
Total DC Current= 86.27 μ A
Figure of Merit(FOM)= 100.74*10⁹Hz/A

B. Common mode STB analysis

Gain= 49.8712db
Phase Margin=83.3384deg

VII. CONCLUSION

A fully differential amplifier with common mode feedback is designed. Simulations have been performed and Phase Margin better than 60degrees is obtained. The layout is designed and LVS net-lists match.

VIII. REFERENCES

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